



a very rough overview...

Astronomical Instrumentation course lecture 7a Dec 15, 2010

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requirements definition

- FOV
- (effective) focal length
- spatial resolution (+ sampling)
- spectral range & resolution (+ sampling)
- polarimetric performance
- transmission
- stability
- etc.



boundary conditions

- telescope
- telescope interfaces (see next lecture)
- focal station dimensions
- focal station gravity vector
- detector availability
- available € or \$



global set-up

- lenses or mirrors (depends on wavelength range)
- choice of dispersing elements (prism, grating)
- location of aperture stop
- locations of image and pupil planes
- sampling (Nyquist: >2 pixels per resolution element)
- (dichroic) beam-splitting
- etc.



global set-up

- (de-)magnification
- F-numbers
 - the amount of problems with aberrations increases with smaller F-number...
- collimated beam?
- telecentric beam?

optical design global set-up



 minimum geometrical aberrations for symmetric system (m=1)



global set-up

- components in collimated beam?
 - dispersion element
 - cold stop
 - Lyot stop
 - filter?
 - polarization modulator?

• components in converging beam?

- slit
- coronagraphic mask
- detector
- filter?



étendue

- or "throughput" or "grasp", connected with "Lagrange invariant" or "optical invariant"
- derived from conservation of energy
- considered in every pupil plane:
 - -3D: aperture*FOV = A* Ω = constant
 - $-2D: d^*\theta = constant$
- unless focal ratio degradation in fibers...

optical design block diagram





optical design block diagram

SPICES







- used in optical design programs:
 - WinLens
 - -ZEMAX
 - OSLO
 - CodeV
 - -etc.
- Such programs are only useful when major design decisions have already been made!



- direction cosines $\mathbf{v}=(\gamma,\delta,\epsilon)$
 - $-\gamma = \cos \theta$
 - $-\delta = \cos \phi$
 - $-\epsilon = \cos \psi$
- propagation along distance s measured in z direction:

$$-x_{2} = \gamma s/\epsilon + x_{1}$$
$$-y_{2} = \delta s/\epsilon + y_{1}$$
$$-z_{2} = s + z_{1}$$

- surface P with normal $\mathbf{v'}=(\gamma',\delta',\epsilon')$
- incidence angle i = $\arccos(\gamma\gamma' + \delta\delta' + \epsilon\epsilon')$
- reflection: $\gamma\gamma$ " + $\delta\delta$ " + $\epsilon\epsilon$ " = cos 2r
- refraction: γγ" + δδ" + εε" = cos (i-r) use Snell's law
- relation with the surface normal: $\gamma'\gamma'' + \delta'\delta'' + \epsilon'\epsilon'' = \cos r$
- plus **v**, **v**' and **v**" should be in one plane: $(\mathbf{v}\mathbf{x}\mathbf{v}')\mathbf{\cdot v}" = 0$ $(\epsilon\delta' - \epsilon'\delta)\gamma" + (\gamma\epsilon' - \gamma'\epsilon)\delta" + (\delta\gamma' - \delta'\gamma)\epsilon" = 0$



- sequential
 - from one surface to the next along the z axis
 - populate the pupil with rays
 - wavelength λ , field [x,y] as global parameters
- non-sequential
 - specific 3D volume and fire off rays in all directions

ray tracing

sequential









• FFT PSF





optical design aberration plots



- transverse / longitudinal aberration
- Seidel diagram



optical design optimization

- variables:
 - positions
 - angles
 - radii of curvature
 - conic constants
 - glass type
 - coating layers and material
 - etc.





optimization

- merit function
- weighted linear combination of:
 - system:
 - effective focal length
 - spot:
 - centroid position
 - RMS radius
 - MTF
 - Strehl ratio (observed peak intensity / maximum peak intensity)
 - encircled energy
 - coating polarization properties
 - etc





design examples







design examples

X-shooter



measured

simulated from optical design







tolerancing

- spot diagram diffraction limited with margin?
- sensitivity analysis for individual elements
- in the end: Monte Carlo

tolerancing







tolerancing

 example: EPICS-EPOL

DECENTERS			TILTS				
	Apodiser						
0.0	0.0	0.0	0.0	0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0		
		Entire teles	соре				
1000.0	0.0	-0.1	0.0	2016.8	10.8		
0.0	1000.0	-0.1	-2016.8	0.0	34.8		
0.0	0.0	-1000.0	0.0	0.0	0.0		
EPOL M1							
14997.8	0.0	520.6	0.0	-4654.0	88.5		
0.0	14997.8	539.5	4654.0	0.0	85.8		
-0.4	0.0	-256224.9	0.0	0.0	0.0		
EPOL M2							
-13997.7	0.0	967.1	0.0	872.5	0.1		
0.0	-13997.7	948.2	-872.5	0.0	0.6		
0.4	0.0	195390.7	0.0	0.0	0.0		
Folding 1							
0.0	0.0	0.0	0.0	-345.3	0.1		
0.0	0.0	0.0	348.9	0.0	0.1		
287.0	0.0	-1979.3	0.0	0.0	0.0		
folding 2							
0.0	0.0	0.0	0.0	194.4	0.1		
0.0	0.0	0.0	-196.5	0.0	0.1		
287.0	0.0	1979.3	0.0	0.0	0.0		



- look at where "second order" light ends up in non-sequential ray tracing
- or light outside FOV (in sequential ray tracing)
- solutions:
 - baffling
 - "ghosts": defocus or tilt surfaces to move outside FOV



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systems engineering why?



- Consider instrument as being more than just sum of its parts (subsystems).
- Crucial for complex instruments.
- Implement from beginning of the project.
- Interaction with optical, mechanical, electronic, software design.
- Interaction between different international teams (interfaces).



- wavefront error
- transmission
- thermal background
- radial velocity
- polarimetric accuracy
- etc.
- financial!



- top-down or bottom-up?
- first: distribution of best guess
- add quadratically or linearly?
- continuously update during design process and evaluate
- identify (critical) issues that contribute substantially to overall degradation of performance, and take action to mitigate

- system
 - subsystem A
 - component 1
 - component 2
 - subsystem B
 - component 3
 - component 4
 - component 5
- total





 observing system imaging performance 	static	dynamic
– seeing		
– telescope		
• M1		
 manufacturing & testing 		
 alignment active optics performance 		
 wind buffeting 		
 pointing & guiding 		
– AO		
 optics wavefront error 		
 wavefront sensor noise influence 		
DM correction		
 non-common path errors 		
 spectrograph 		
flexure		
detector focusing		

systems engineering WFE budget



- magnitude of error in [nm]
- decomposition in spatial frequencies or Zernike polynomials
- location: close to pupil plane or image plane?
- sensitivity analysis in optical design to assess whether or not a certain error is critical

WFE budget

sensitivities from ZEMAX:

	۸ .	Dup	
	(%)	ΔX/Φ (%)	WFE RMS (in nm)
Dx EPOL M1	0.6		52.9
Dy EPOL M1		0.3	52.8
Dz EPOL M1	0.1		909.6
Tx EPOL M1	1.2	0.6	49.3
Ty EPOL M1			49.3
TFRN EPOL M1			72.7
Dx EPOL M2	0.9		52.8
Dy EPOL M2		0.5	52.8
Dz EPOL M2	0.01		912.1
Tx EPOL M2	0.3	0.2	9.2
Ty EPOL M2			9.3
TFRN EPOL M2			59.8
Tx folding 1	1.4	0.7	0.1
Dz folding 1	0.01		8.2
TFRN folding 1			21.2
Tx folding 2	1.7	0.8	0.1
Dz folding 2			8.2
TFRN folding 2			9.2

overall:			∆s in nm	Number of surface	Materials interface	index of refraction difference	∆w for each component in nm	PV spec nm in wave at 633 nm
	Polarization compensator		13.9	2	Fused Silica-Air	0.455	9.0	20
	HWP-Z		19.0				9.0	20
		Surface1	9.5	1	Air-Quartz	0.541		
		Surface2	9.5	1	Quartz-Air	0.541		
		Surface3	9.5	1	Air-MgF2	0.376		
		Surface4	9.5	1	MgF2-Air	0.376		
	Window FLC		26.9	2			8.9	20
	Housing	Surface1	19	1	Air-Fused Silica	0.455		
S (in nm)		Surface2	19	1	Fused Silica- Cement_NOA61	0.108		
2.9	Zero		24.0				9.3	20
2.8 9.6	order plate	Surface1	17	1	Cement_NOA61- Quarzt	0.022		
9.3		Surface2	17	1	Quartz-Air	0.541		
9.3	FLC		9.2	2	Fused Silica-Air	0.455	6.0	30
2.7	Window FLC Housing		13.9	2	Fused Silica-Air	0.455	9.0	20
2.8	Beam Splitter	Surface1	14.0	1	Air-N-SF15	0.689	9.7	19
2.0		Surface2	14.0	1	Air-N-SF15		9.7	19
2.1	Filter 1		28.0	2	Fused Silica-Air	0.455	18.1	10
.2	Camera Lens		26.0				8.9	20
.3		Surface1	13	1	Air-S-NSL36	0.513		
.1		Surface2	13	1	S-NSL36- Cement_NOA61	0.050		
.2		Surface3	13	1	Cement_NOA61- CAF2	0.153		
1		Surface4	13	1	CAF2-Air	0.410		
2	Filter 2		28.0	2	Fused Silica-Air	0.455	18.1	10
.2	Field Lens		14.0	2	Caf2-Air	0.410	8.1	22
						Total WFE in nm	37.9	



interaction w/ mechanical design

- mounting precision [x,y,x], [φ,χ,ψ] from optical design
- optics deformation from mechanical design and finite element modeling
- several iterations of loop between optical and mechanical design



cryogenic instruments

- alignment at room temperature
- contraction and deformation due to cool-down
- cryogenic alignment mechanisms
- ZEMAX allows for lengths to be determined by metal at certain temperature
- mirrors, mounts and bench out of aluminum: focus invariant
- invar material



transmission budget

- reduce number of surfaces (>1% loss per surface)
- optimize coatings
- main ingredient for photon budget, plus photon noise and readout noise
- exposure time calculator: S/N for science goal feasible within a night?

systems engineering transmission budget



1.0 SOLAR INPUT TELESCOPE NO. 2 FLAT 0.8 Intrance Window No. 3 Concave 0.6 NO.4 FLAT Exit Window ield Lens 0.4 LITTROW LENS SPECTROGRAPH 0.2 GRATING FILTER MAGNETOGRAPH KERR CELL 0.1 -λ/4 PLATE 0.08 0.06 POLAROID 0.04 EXIT SLIT DIODE FLAT DIODE LENS 0.02 0.0 0.4 0.6 0.8 1.0 1.2 µm λ





systems engineering controlling complexity

- number of moving parts
- thermal control
- vacuum systems
- number of observing modes
- deal with single-point failures
 - redundancy



requirements verification

- verification matrix for lab tests
- traceability to science requirements
 - What is the science impact if a certain spec cannot be achieved?