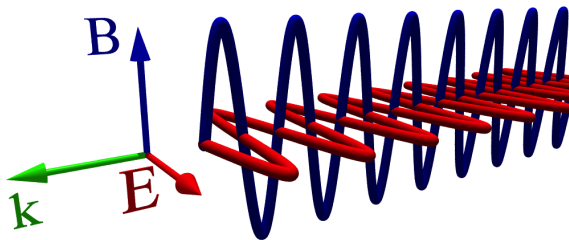


## Outline

- 1 Polarized Light in the Universe
- 2 Brewster Angle and Total Internal Reflection
- 3 Descriptions of Polarized Light
- 4 Polarizers
- 5 Retarders

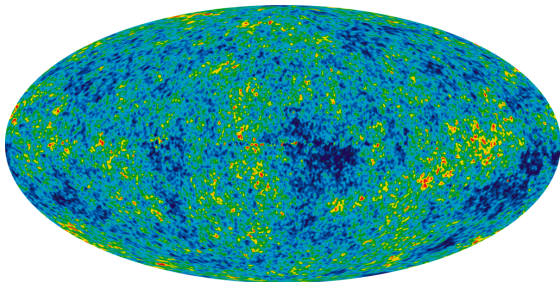


*Polarization* indicates *anisotropy*  $\Rightarrow$  not all directions are equal

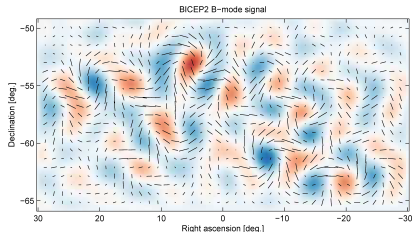
Typical anisotropies introduced by

- geometry (not everything is spherically symmetric)
- temperature gradients
- density gradients
- magnetic fields
- electrical fields

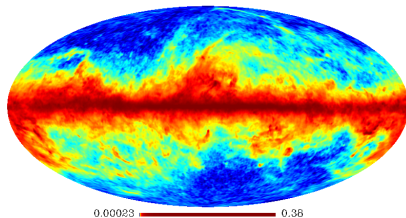
## 13.7 billion year old temperature fluctuations from WMAP



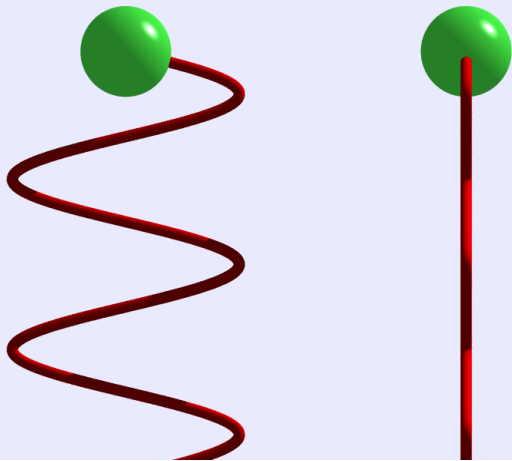
## BICEP2 results and Planck Dust Polarization Map



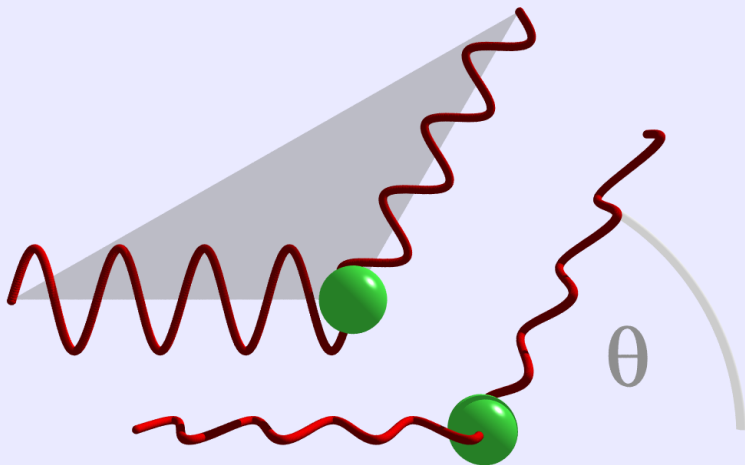
I map 1deg resolution



## Scattering Polarization 1

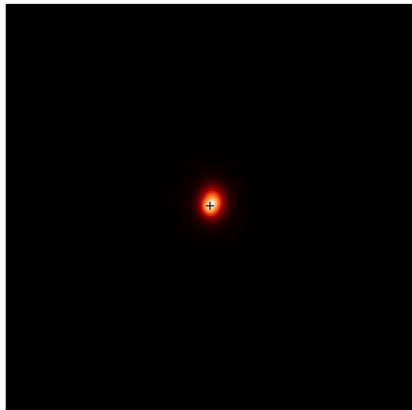


## Scattering Polarization 2

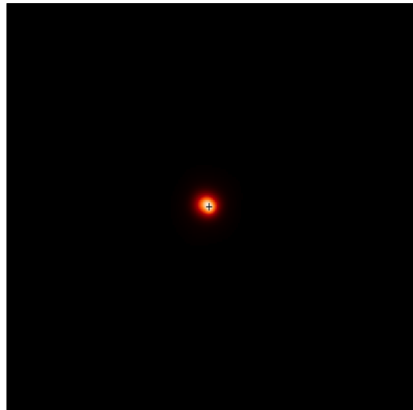


## The Power of Polarimetry

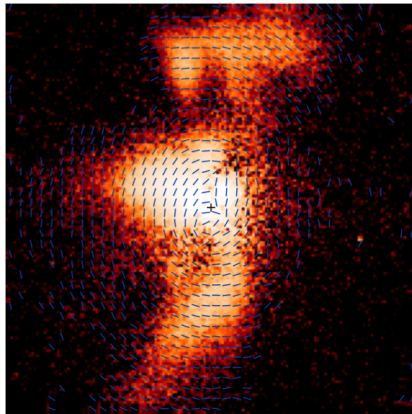
T Tauri in intensity



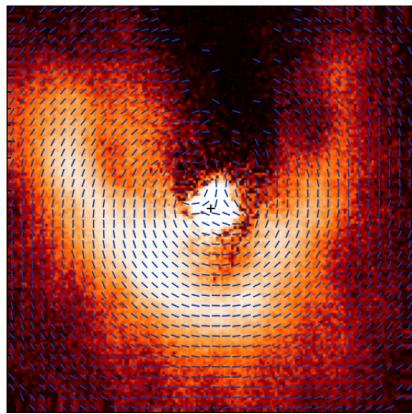
MWC147 in intensity



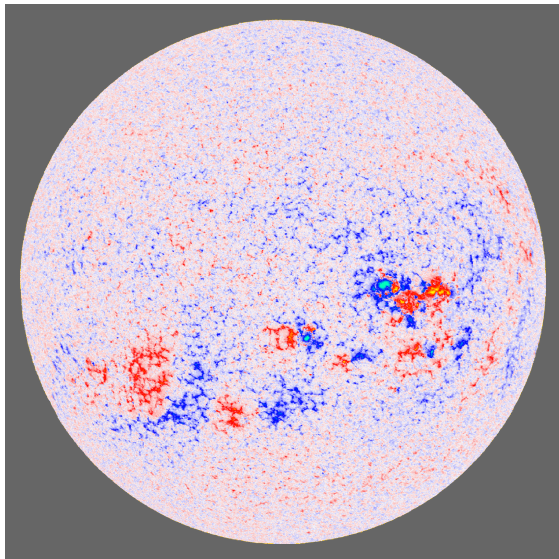
T Tauri in Linear Polarization



MWC147 in Linear Polarization



## Solar Magnetic Field Maps from Longitudinal Zeeman Effect





## Summary of Polarization Origin

- Plane Vector Wave ansatz  $\vec{E} = \vec{E}_0 e^{i(\vec{k}\cdot\vec{x}-\omega t)}$
- spatially, temporally constant vector  $\vec{E}_0$  lays in plane perpendicular to propagation direction  $\vec{k}$
- represent  $\vec{E}_0$  in 2-D basis, unit vectors  $\vec{e}_x$  and  $\vec{e}_y$ , both perpendicular to  $\vec{k}$

$$\vec{E}_0 = E_x \vec{e}_x + E_y \vec{e}_y.$$

$E_x, E_y$ : arbitrary complex scalars

- damped plane-wave solution with given  $\omega, \vec{k}$  has 4 degrees of freedom (two complex scalars)
- additional property is called *polarization*
- many ways to represent these four quantities
- if  $E_1$  and  $E_2$  have identical phases,  $\vec{E}$  oscillates in fixed plane

## Summary of Fresnel Equations

- electric field amplitude transmission  $t_{s,p}$ , reflection  $r_{s,p}$

$$t_s = \frac{2\tilde{n}_1 \cos \theta_i}{\tilde{n}_1 \cos \theta_i + \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}$$

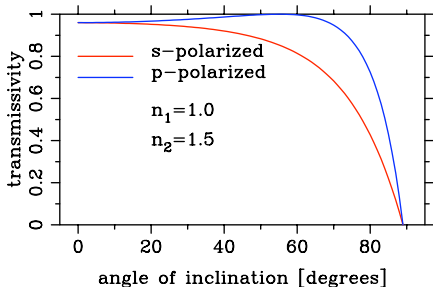
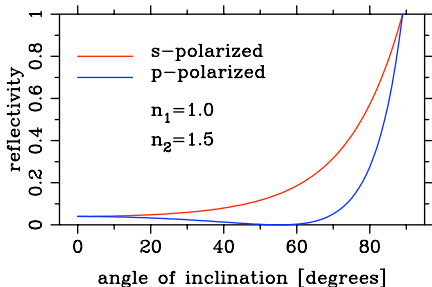
$$t_p = \frac{2\tilde{n}_1 \tilde{n}_2 \cos \theta_i}{\tilde{n}_2^2 \cos \theta_i + \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}$$

$$r_s = \frac{\tilde{n}_1 \cos \theta_i - \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}{\tilde{n}_1 \cos \theta_i + \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}$$

$$r_p = \frac{\tilde{n}_2^2 \cos \theta_i - \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}{\tilde{n}_2^2 \cos \theta_i + \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2 \theta_i}}$$

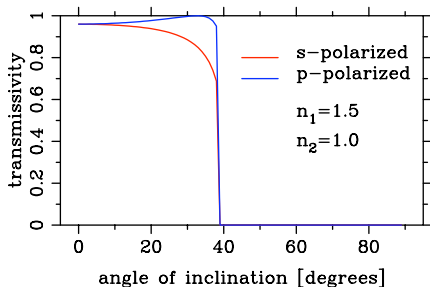
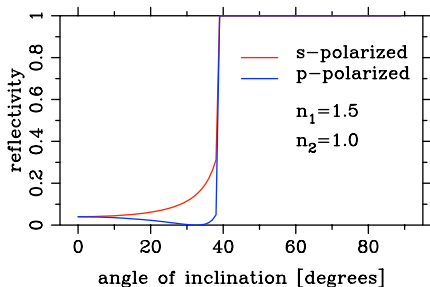
- reflectivity:  $R = |r_{s,p}|^2$ , transmissivity:  $T = \frac{|\tilde{n}_2| \cos \theta_t}{|\tilde{n}_1| \cos \theta_i} |t_{s,p}|^2$

## Brewster Angle



- $r_p = \frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)} = 0$  when  $\theta_i + \theta_t = \frac{\pi}{2}$
- corresponds to *Brewster angle* of incidence of  $\tan \theta_B = \frac{n_2}{n_1}$
- occurs when reflected wave is perpendicular to transmitted wave
- reflected light is completely s-polarized
- transmitted light is moderately polarized

## Total Internal Reflection (TIR)



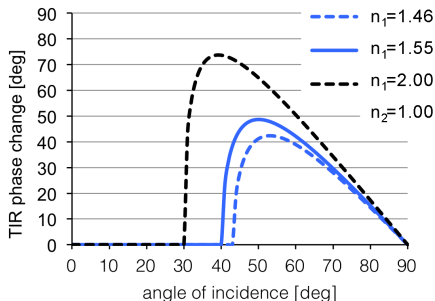
- Snell's law:  $\sin \theta_t = \frac{n_1}{n_2} \sin \theta_i$
- wave from high-index medium into lower index medium (e.g. glass to air):  $n_1/n_2 > 1$
- right-hand side  $> 1$  for  $\sin \theta_i > \frac{n_2}{n_1}$
- all light is reflected in high-index medium  $\Rightarrow$  *total internal reflection*
- transmitted wave has complex phase angle  $\Rightarrow$  damped wave along interface

## Phase Change on Total Internal Reflection (TIR)

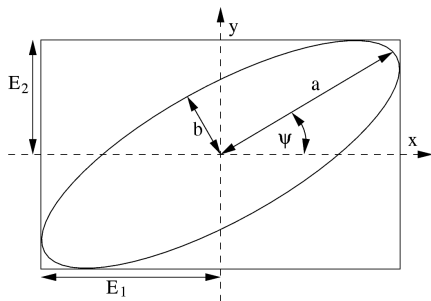
- TIR induces phase change that depends on polarization
- complex ratios:  
 $r_{s,p} = |r_{s,p}| e^{i\delta_{s,p}}$
- phase change  $\delta = \delta_s - \delta_p$

$$\tan \frac{\delta}{2} = \frac{\cos \theta_i \sqrt{\sin^2 \theta_i - \left(\frac{n_2}{n_1}\right)^2}}{\sin^2 \theta_i}$$

- relation valid between critical angle and grazing incidence
- at critical angle and grazing incidence  $\delta = 0$



## Polarization Ellipse



## Polarization

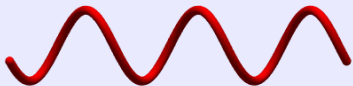
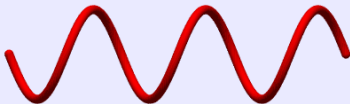
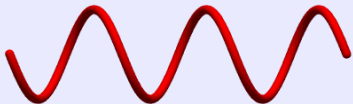
$$\vec{E}(t) = \vec{E}_0 e^{i(\vec{k} \cdot \vec{x} - \omega t)}$$

$$\vec{E}_0 = |E_x| e^{i\delta_x} \vec{e}_x + |E_y| e^{i\delta_y} \vec{e}_y$$

- wave vector in z-direction
- $\vec{e}_x, \vec{e}_y$ : unit vectors in x, y
- $|E_x|, |E_y|$ : (real) amplitudes
- $\delta_{x,y}$ : (real) phases

## Polarization Description

- 2 complex scalars not the most useful description
- at given  $\vec{x}$ , time evolution of  $\vec{E}$  described by *polarization ellipse*
- ellipse described by axes  $a, b$ , orientation  $\psi$



## Jones Vectors

$$\vec{E}_0 = E_x \vec{e}_x + E_y \vec{e}_y$$

- beam in z-direction
- $\vec{e}_x, \vec{e}_y$  unit vectors in x, y-direction
- complex scalars  $E_{x,y}$
- Jones vector

$$\vec{e} = \begin{pmatrix} E_x \\ E_y \end{pmatrix}$$

- phase difference between  $E_x, E_y$  multiple of  $\pi$ , electric field vector oscillates in a fixed plane  $\Rightarrow$  *linear polarization*
- phase difference  $\pm \frac{\pi}{2} \Rightarrow$  *circular polarization*



$$\vec{E}_0 = E_x \vec{e}_x + E_y \vec{e}_y$$

$$\vec{e} = \begin{pmatrix} E_x \\ E_y \end{pmatrix}$$

- Maxwell's equations linear  $\Rightarrow$  sum of two solutions again a solution
- Jones vector of sum of two waves = sum of Jones vectors of individual waves if wave vectors  $\vec{k}$  the same
- addition of Jones vectors: *coherent* superposition of waves
- elements of Jones vectors are not observed directly
- observables always depend on products of elements of Jones vectors, i.e. intensity

$$I = \vec{e} \cdot \vec{e}^* = e_x e_x^* + e_y e_y^*$$

## Jones matrices

- influence of medium on polarization described by  $2 \times 2$  complex *Jones matrix*  $J$

$$\vec{e}' = J\vec{e} = \begin{pmatrix} J_{11} & J_{12} \\ J_{21} & J_{22} \end{pmatrix} \vec{e}$$

- assumes that medium not affected by polarization state
- different media 1 to  $N$  in order of wave direction  $\Rightarrow$  combined influence described by

$$J = J_N J_{N-1} \cdots J_2 J_1$$

- order of matrices in product is crucial
- Jones calculus describes coherent superposition of polarized light

## Linear Polarization

- horizontal:  $\begin{pmatrix} 1 \\ 0 \end{pmatrix}$
- vertical:  $\begin{pmatrix} 0 \\ 1 \end{pmatrix}$
- $45^\circ$ :  $\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$

## Circular Polarization

- left:  $\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}$
- right:  $\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -i \end{pmatrix}$

## Notes on Jones Formalism

- Jones formalism operates on amplitudes, not intensities
- coherent superposition important for coherent light (lasers, interference effects)
- Jones formalism describes 100% polarized light

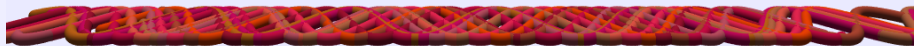
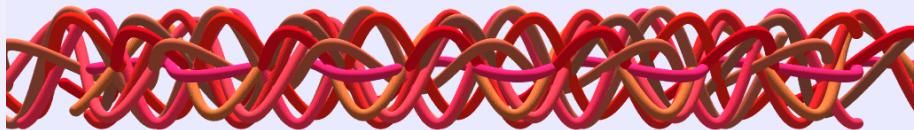
## Stokes Vector

- formalism to describe polarization of quasi-monochromatic light
- directly related to measurable intensities
- Stokes vector fulfills these requirements

$$\vec{I} = \begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix} = \begin{pmatrix} E_x E_x^* + E_y E_y^* \\ E_x E_x^* - E_y E_y^* \\ E_x E_y^* + E_y E_x^* \\ i(E_x E_y^* - E_y E_x^*) \end{pmatrix} = \begin{pmatrix} |E_x|^2 + |E_y|^2 \\ |E_x|^2 - |E_y|^2 \\ 2|E_x||E_y| \cos \delta \\ 2|E_x||E_y| \sin \delta \end{pmatrix}$$

Jones vector elements  $E_{x,y}$ , real amplitudes  $|E_{x,y}|$ , phase difference  $\delta = \delta_y - \delta_x$

- $I^2 \geq Q^2 + U^2 + V^2$
- can describe unpolarized ( $Q = U = V = 0$ ) light



## Stokes Vector Interpretation

$$\vec{I} = \begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix} = \begin{pmatrix} \text{intensity} \\ \text{linear } 0^\circ - \text{linear } 90^\circ \\ \text{linear } 45^\circ - \text{linear } 135^\circ \\ \text{circular left} - \text{right} \end{pmatrix}$$

- *degree of polarization*

$$P = \frac{\sqrt{Q^2 + U^2 + V^2}}{I}$$

1 for fully polarized light, 0 for unpolarized light

- summing of Stokes vectors = *incoherent* adding of quasi-monochromatic light waves

## Linear Polarization

- horizontal:  $\begin{pmatrix} 1 \\ -1 \\ 0 \\ 0 \end{pmatrix}$

- vertical:  $\begin{pmatrix} 1 \\ 1 \\ 0 \\ 0 \end{pmatrix}$

- $45^\circ$ :  $\begin{pmatrix} 1 \\ 0 \\ 1 \\ 0 \end{pmatrix}$

## Circular Polarization

- left:  $\begin{pmatrix} 1 \\ 0 \\ 0 \\ 1 \end{pmatrix}$

- right:  $\begin{pmatrix} 1 \\ 0 \\ 0 \\ -1 \end{pmatrix}$

## Mueller Matrices

- $4 \times 4$  real Mueller matrices describe (linear) transformation between Stokes vectors when passing through or reflecting from media

$$\vec{I}' = M\vec{I},$$

$$M = \begin{pmatrix} M_{11} & M_{12} & M_{13} & M_{14} \\ M_{21} & M_{22} & M_{23} & M_{24} \\ M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{pmatrix}$$

- $N$  optical elements, combined Mueller matrix is

$$M' = M_N M_{N-1} \cdots M_2 M_1$$



## Rotating Mueller Matrices

- optical element with Mueller matrix  $M$
- Mueller matrix of the same element rotated by  $\theta$  around the beam given by

$$M(\theta) = R(-\theta)MR(\theta)$$

with

$$R(\theta) = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2\theta & \sin 2\theta & 0 \\ 0 & -\sin 2\theta & \cos 2\theta & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

### Vertical Linear Polarizer

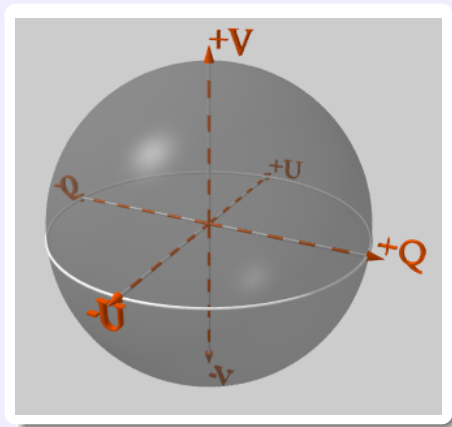
$$M_{\text{pol}}(\theta) = \frac{1}{2} \begin{pmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

### Horizontal Linear Polarizer

$$M_{\text{pol}}(\theta) = \frac{1}{2} \begin{pmatrix} 1 & -1 & 0 & 0 \\ -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

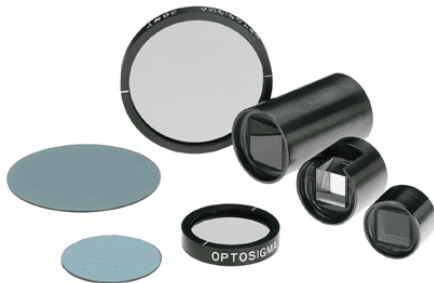
### Mueller Matrix for Ideal Linear Polarizer at Angle $\theta$

$$M_{\text{pol}}(\theta) = \frac{1}{2} \begin{pmatrix} 1 & \cos 2\theta & \sin 2\theta & 0 \\ \cos 2\theta & \cos^2 2\theta & \sin 2\theta \cos 2\theta & 0 \\ \sin 2\theta & \sin 2\theta \cos 2\theta & \sin^2 2\theta & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$



## Relation to Stokes Vector

- fully polarized light:  
 $I^2 = Q^2 + U^2 + V^2$
- for  $I^2 = 1$ : sphere in  $Q, U, V$  coordinate system
- point on Poincaré sphere represents particular state of polarization
- graphical representation of fully polarized light



- polarizer: optical element that produces polarized light from unpolarized input light
- linear, circular, or in general elliptical polarizer, depending on type of transmitted polarization
- linear polarizers by far the most common
- large variety of polarizers

## Jones Matrix for Linear Polarizers

- Jones matrix for linear polarizer:

$$J_p = \begin{pmatrix} p_x & 0 \\ 0 & p_y \end{pmatrix}$$

- $0 \leq p_x \leq 1$  and  $0 \leq p_y \leq 1$ , real: transmission factors for x, y-components of electric field:  $E'_x = p_x E_x$ ,  $E'_y = p_y E_y$
- $p_x = 1$ ,  $p_y = 0$ : linear polarizer in  $+Q$  direction
- $p_x = 0$ ,  $p_y = 1$ : linear polarizer in  $-Q$  direction
- $p_x = p_y$ : neutral density filter

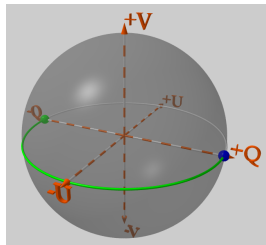
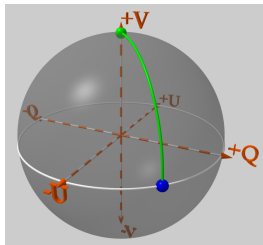
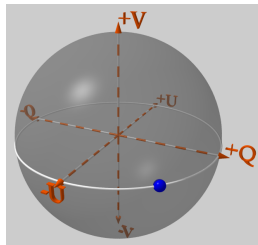
## Mueller Matrix for Linear Polarizers

$$M_p = \frac{1}{2} \begin{pmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

## Mueller Matrix for Ideal Linear Polarizer at Angle $\theta$

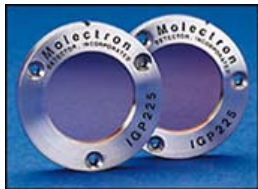
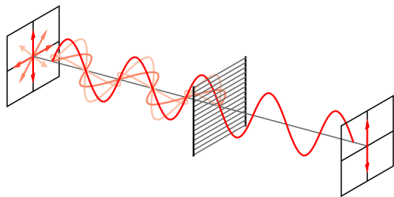
$$M_{\text{pol}}(\theta) = \frac{1}{2} \begin{pmatrix} 1 & \cos 2\theta & \sin 2\theta & 0 \\ \cos 2\theta & \cos^2 2\theta & \sin 2\theta \cos 2\theta & 0 \\ \sin 2\theta & \sin 2\theta \cos 2\theta & \sin^2 2\theta & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

## Poincaré Sphere



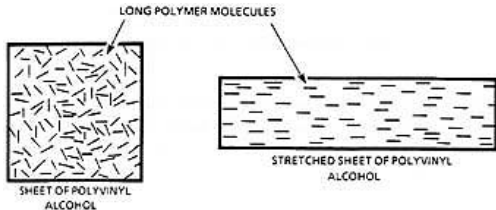
- polarizer is a point on the Poincaré sphere
- transmitted intensity:  $\cos^2(l/2)$ ,  $l$  is arch length of great circle between incoming polarization and polarizer on Poincaré sphere

## Wire Grid Polarizers



- parallel conducting wires, spacing  $d \lesssim \lambda$  act as polarizer
- electric field parallel to wires induces electrical currents in wires
- induced electrical current reflects polarization parallel to wires
- polarization perpendicular to wires is transmitted
- rule of thumb:
  - $d < \lambda/2 \Rightarrow$  strong polarization
  - $d \gg \lambda \Rightarrow$  high transmission of both polarization states (weak polarization)
- mostly used in infrared

## Polaroid-type Polarizers



- developed by Edwin Land in 1938  $\Rightarrow$  Polaroid
- sheet polarizers: stretched polyvynil alcohol (PVA) sheet, laminated to sheet of cellulose acetate butyrate, treated with iodine
- PVA-iodine complex analogous to short, conducting wire
- cheap, can be manufactured in large sizes



## Properties of Dielectric Tensor

- Maxwell equations imply symmetric dielectric tensor

$$\epsilon = \epsilon^T = \begin{pmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{12} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{13} & \epsilon_{23} & \epsilon_{33} \end{pmatrix}$$

- symmetric tensor of rank 2  $\Rightarrow$  coordinate system exists where tensor is diagonal
- orthogonal axes of this coordinate system: *principal axes*
- elements of diagonal tensor: *principal dielectric constants*
- 3 *principal indices of refraction* in coordinate system spanned by principal axes

$$\vec{D} = \begin{pmatrix} n_x^2 & 0 & 0 \\ 0 & n_y^2 & 0 \\ 0 & 0 & n_z^2 \end{pmatrix} \vec{E}$$

- $x, y, z$  because principal axes form Cartesian coordinate system

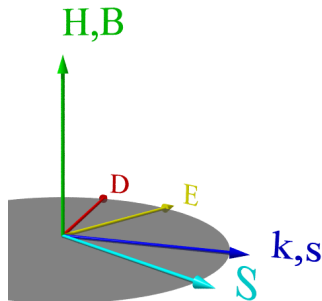
## Uniaxial Materials

- isotropic materials:  $n_x = n_y = n_z$
- anisotropic materials:  
 $n_x \neq n_y \neq n_z$
- *uniaxial materials*:  $n_x = n_y \neq n_z$
- *ordinary index of refraction*:  
 $n_o = n_x = n_y$
- *extraordinary index of refraction*:  
 $n_e = n_z$
- rotation of coordinate system around  $z$  has no effect
- most materials used in polarimetry are (almost) uniaxial



## Plane Waves in Anisotropic Media

- no net charges ( $\nabla \cdot \vec{D} = 0$ ):  $\vec{D} \cdot \vec{k} = 0$
- $\vec{D} \parallel \vec{E} \Rightarrow \vec{E} \not\parallel \vec{k}$
- constant, scalar  $\mu$ , vanishing current density  $\Rightarrow \vec{H} \parallel \vec{B}$
- $\nabla \cdot \vec{H} = 0 \Rightarrow \vec{H} \perp \vec{k}$
- $\nabla \times \vec{H} = \frac{1}{c} \frac{\partial \vec{D}}{\partial t} \Rightarrow \vec{H} \perp \vec{D}$
- $\nabla \times \vec{E} = -\frac{\mu}{c} \frac{\partial \vec{H}}{\partial t} \Rightarrow \vec{H} \perp \vec{E}$
- $\vec{D}$ ,  $\vec{E}$ , and  $\vec{k}$  all in one plane
- $\vec{H}$ ,  $\vec{B}$  perpendicular to that plane
- Poynting vector  $\vec{S} = \frac{c}{4\pi} \vec{E} \times \vec{H}$   
perpendicular to  $\vec{E}$  and  $\vec{H} \Rightarrow \vec{S}$  (in general) not parallel to  $\vec{k}$
- energy (in general) not transported in direction of wave vector  $\vec{k}$

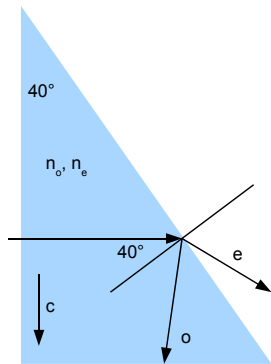


## Phase Delay between Ordinary and Extraordinary Rays

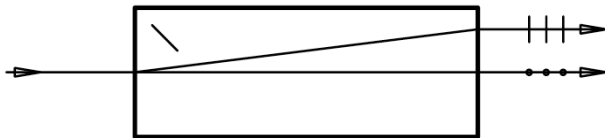
- ordinary and extraordinary wave propagate in same direction
- ordinary ray propagates with speed  $\frac{c}{n_o}$
- extraordinary beam propagates at different speed  $\frac{c}{n_e}$
- $\vec{E}_o, \vec{E}_e$  perpendicular to each other  $\Rightarrow$  plane wave with arbitrary polarization can be (coherently) decomposed into components parallel to  $\vec{E}_o$  and  $\vec{E}_e$
- 2 components will travel at different speeds
- (coherently) superposing 2 components after distance  $d \Rightarrow$  phase difference between 2 components  $\frac{\omega}{c}(n_e - n_o)d$  radians
- phase difference  $\Rightarrow$  change in polarization state
- basis for constructing linear retarders

## Total Internal Reflection (TIR) in Crystals

- TIR also in anisotropic media
- $n_o \neq n_e \Rightarrow$  one beam may be totally reflected while other is transmitted
- principal of most crystal polarizers
- example: calcite prism, normal incidence, optic axis parallel to first interface, exit face inclined by  $40^\circ$
- $\Rightarrow$  extraordinary ray not refracted, two rays propagate according to indices  $n_o, n_e$
- at second interface rays (and wave vectors) at  $40^\circ$  to surface
- 632.8 nm:  $n_o = 1.6558$ ,  $n_e = 1.4852$
- requirement for total reflection  $\frac{n_U}{n_I} \sin \theta_U > 1$
- with  $n_I = 1 \Rightarrow$  extraordinary ray transmitted, ordinary ray undergoes TIR

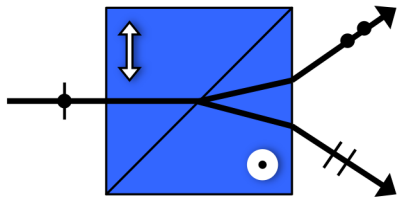


## Crystal-Based Polarizers

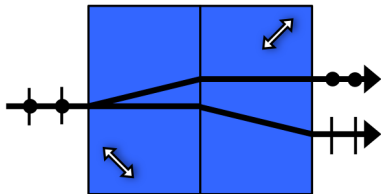


- crystals are basis of highest-quality polarizers
- precise arrangement of atom/molecules and anisotropy of index of refraction separate incoming beam into two beams with precisely orthogonal linear polarization states
- work well over large wavelength range
- many different configurations
- calcite most often used in crystal-based polarizers because of large birefringence, low absorption in visible
- many other suitable materials

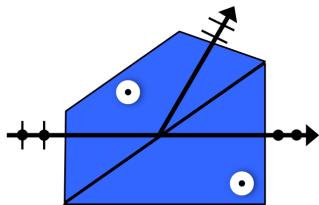
## Wollaston Prism



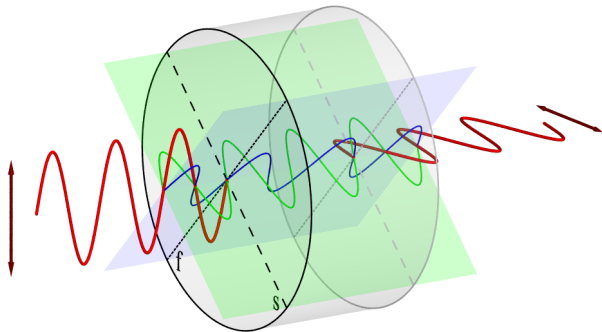
## Savart Plate



## Foster Prism



## Retarders or Wave Plates



- retards (delays) phase of one electric field component with respect to orthogonal component
- anisotropic material (crystal) has index of refraction that depends on polarization



## Retarder Properties

- does not change intensity or degree of polarization
- characterized by two (not identical, not trivial) Stokes vectors of incoming light that are not changed by retarder  $\Rightarrow$  *eigenvectors* of retarder
- depending on polarization described by eigenvectors, retarder is
  - *linear retarder*
  - *circular retarder*
  - *elliptical retarder*
- linear, circular retarders are special cases of elliptical retarders
- circular retarders sometimes called *rotators* since they rotate the orientation of linearly polarized light
- linear retarders by far the most common type of retarder

## Jones Matrix for Linear Retarders

- linear retarder with fast axis at  $0^\circ$  characterized by Jones matrix

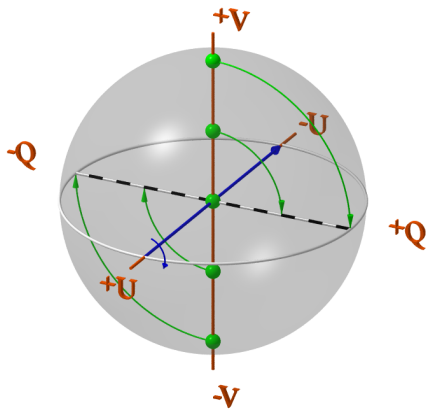
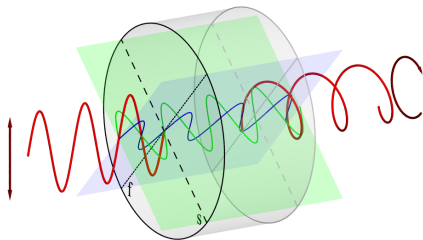
$$J_r(\delta) = \begin{pmatrix} e^{i\delta} & 0 \\ 0 & 1 \end{pmatrix}, \quad J_r(\delta) = \begin{pmatrix} e^{i\frac{\delta}{2}} & 0 \\ 0 & e^{-i\frac{\delta}{2}} \end{pmatrix}$$

- $\delta$ : phase shift between two linear polarization components (in radians)
- absolute phase does not matter

## Mueller Matrix for Linear Retarder

$$M_r = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & \cos \delta & -\sin \delta \\ 0 & 0 & \sin \delta & \cos \delta \end{pmatrix}$$

## Quarter-Wave Plate on the Poincaré Sphere

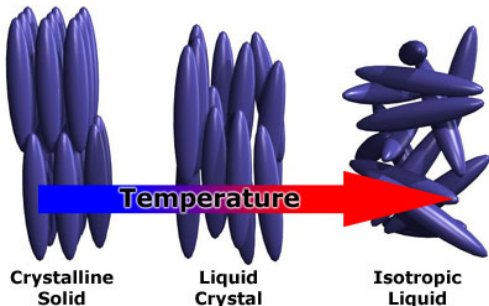


- retarder eigenvector (fast axis) in Poincaré sphere
- points on sphere are rotated around retarder axis by amount of retardation

## Variable Retarders

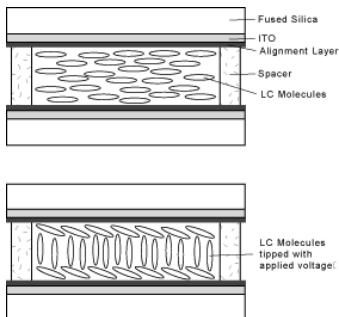
- sensitive polarimeters requires retarders whose properties (retardance, fast axis orientation) can be varied quickly (*modulated*)
- retardance changes (change of birefringence):
  - liquid crystals
  - Faraday, Kerr, Pockels cells
  - piezo-elastic modulators (PEM)
- fast axis orientation changes (change of *c*-axis direction):
  - rotating fixed retarder
  - ferro-electric liquid crystals (FLC)

## Liquid Crystals



- liquid crystals: fluids with elongated molecules
- at high temperatures: liquid crystal is isotropic
- at lower temperature: molecules become ordered in orientation and sometimes also space in one or more dimensions
- liquid crystals can line up parallel or perpendicular to external electrical field

## Liquid Crystal Retarders



- dielectric constant anisotropy often large  $\Rightarrow$  very responsive to changes in applied electric field
- birefringence  $\delta n$  can be very large (larger than typical crystal birefringence)
- liquid crystal layer only a few  $\mu\text{m}$  thick
- birefringence shows strong temperature dependence