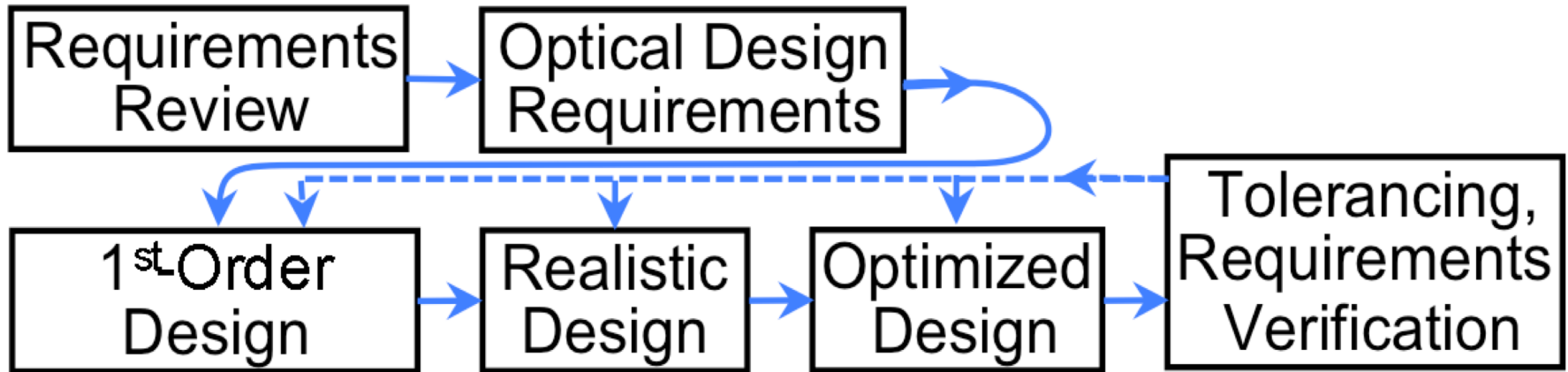


Optical Design

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Optical Design Life Cycle



- Optical design is not linear, but iterative process
- Close coupling between optical, mechanical, electrical, controls, software design and science
- Optical design is *first design effort*, provides first idea of how final instrument will look

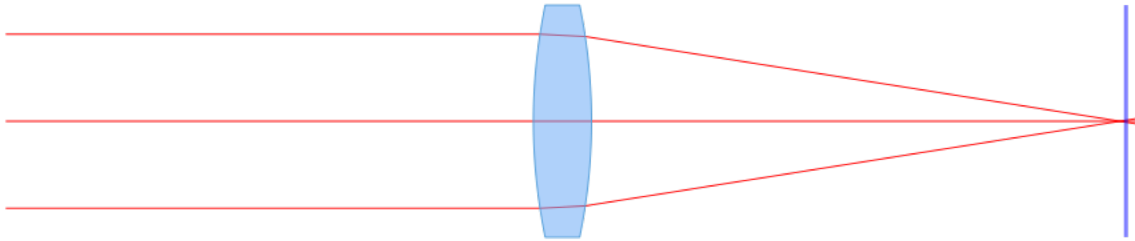
Requirements

- Common optical requirements
 - field-of-view & angular resolution
 - spectral range & resolution, transmission
- Common boundary conditions
 - telescope interfaces & instrument location
 - cooling, weight limit, size limit, cost, schedule, ...
 - detector pixel size
- Review requirements
 - completeness, consistency

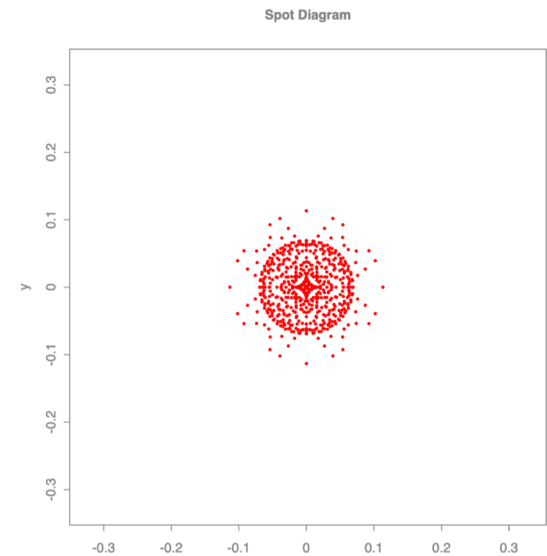
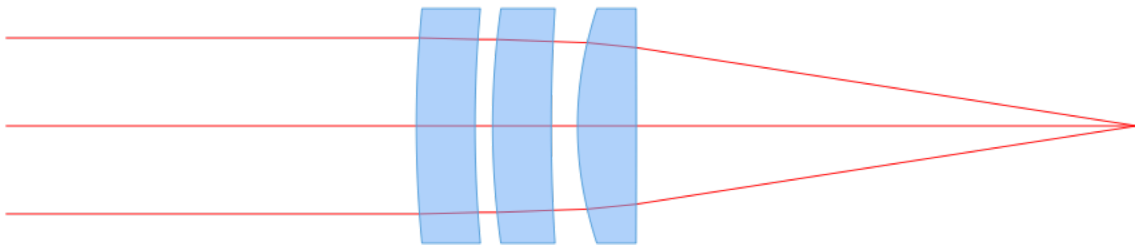
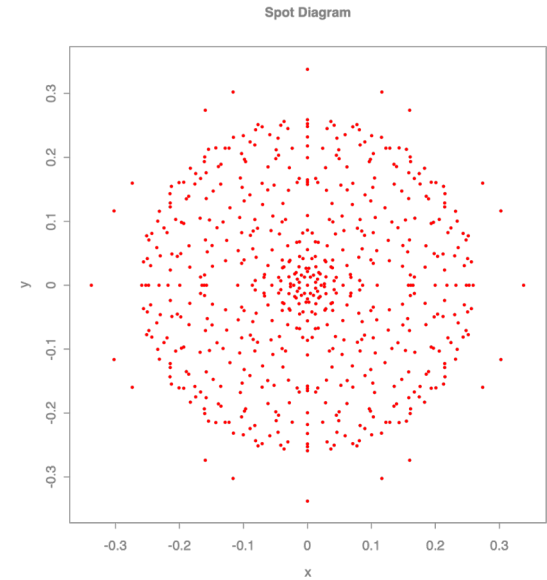
Optical Design Principles 1 - 3

1. Minimize the number of optical components
 - additional elements add cost, ghosts, scattered light
 - but: additional elements increase performance
2. Maximize the radii of curvature
 - reduces aberrations
 - eases manufacturing and alignment
 - but: might require more elements and long designs
3. Maximize the allowed tolerances
 - simplifies manufacturing, mechanical design and operational requirements

Better Performance with More Optics



made with Touch Optical Design version 0.40.0 pro



made with Touch Optical Design version 0.40.0 pro

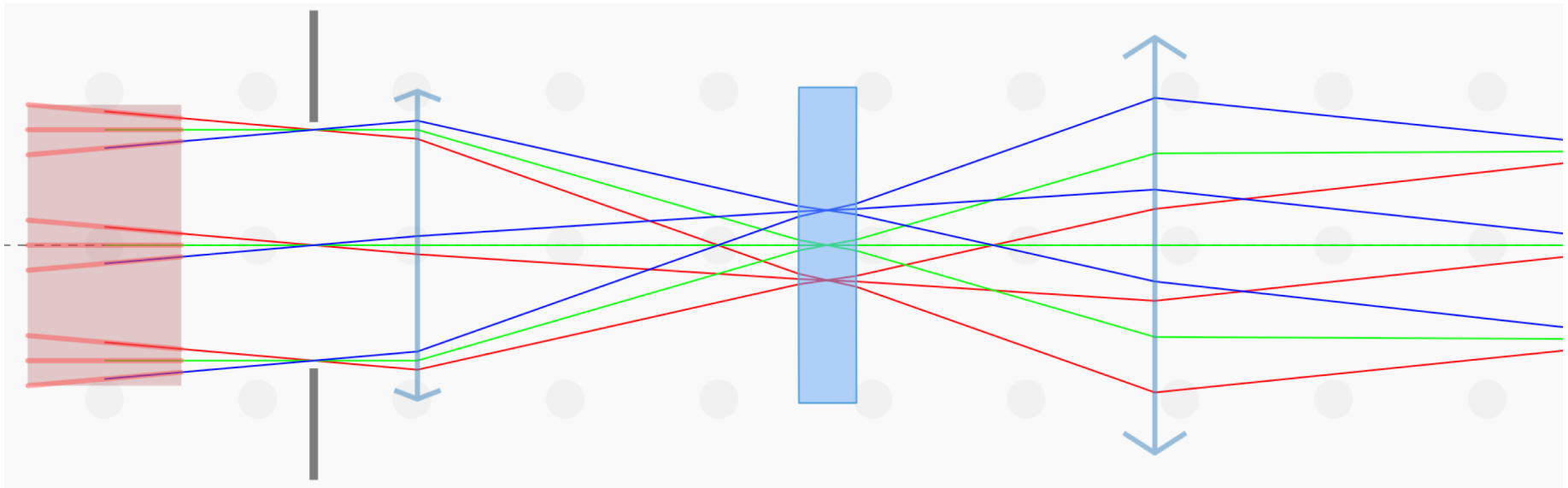
Optical Design Principles 4 - 7

4. Place components close to focus if they introduce wavefront aberrations
5. Place components close to pupil if all field points must pass the same part of component
6. Place components in collimated beam if all rays from one field point should pass the component under the same inclination angle
7. Place components in a telecentric beam if the component is sensitive to the inclination angle

Collimated vs. Converging Beam

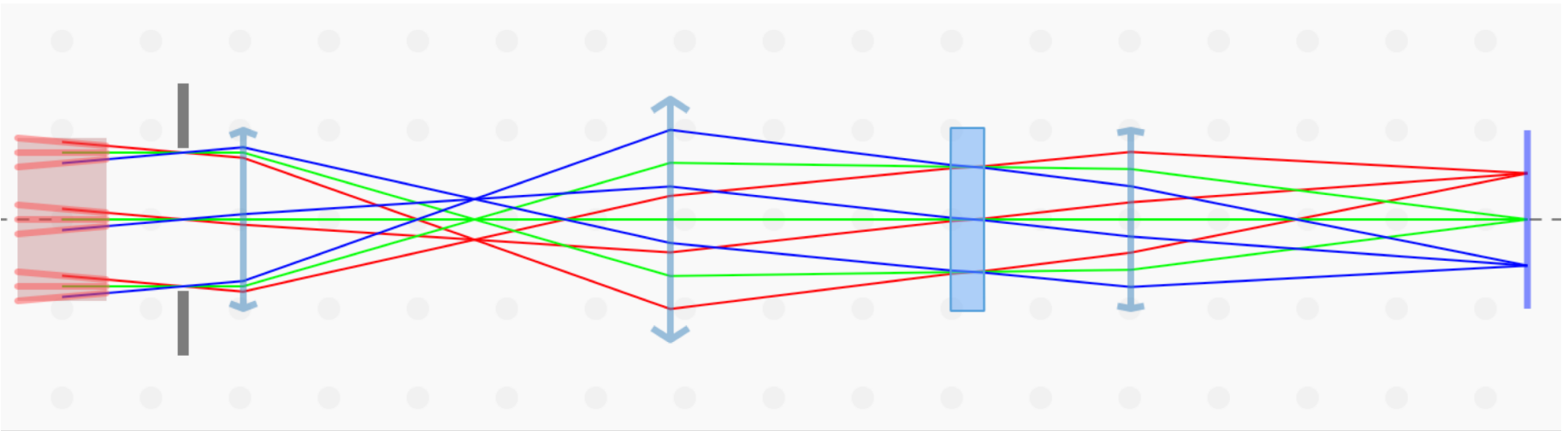
- Components in collimated beam
 - grating, prism
 - cold stop
 - Lyot stop
 - filter?
 - polarization modulator?
- Components in converging beam
 - slit
 - coronagraphic mask
 - detector
 - filter?

Example: Interference Filter in Image



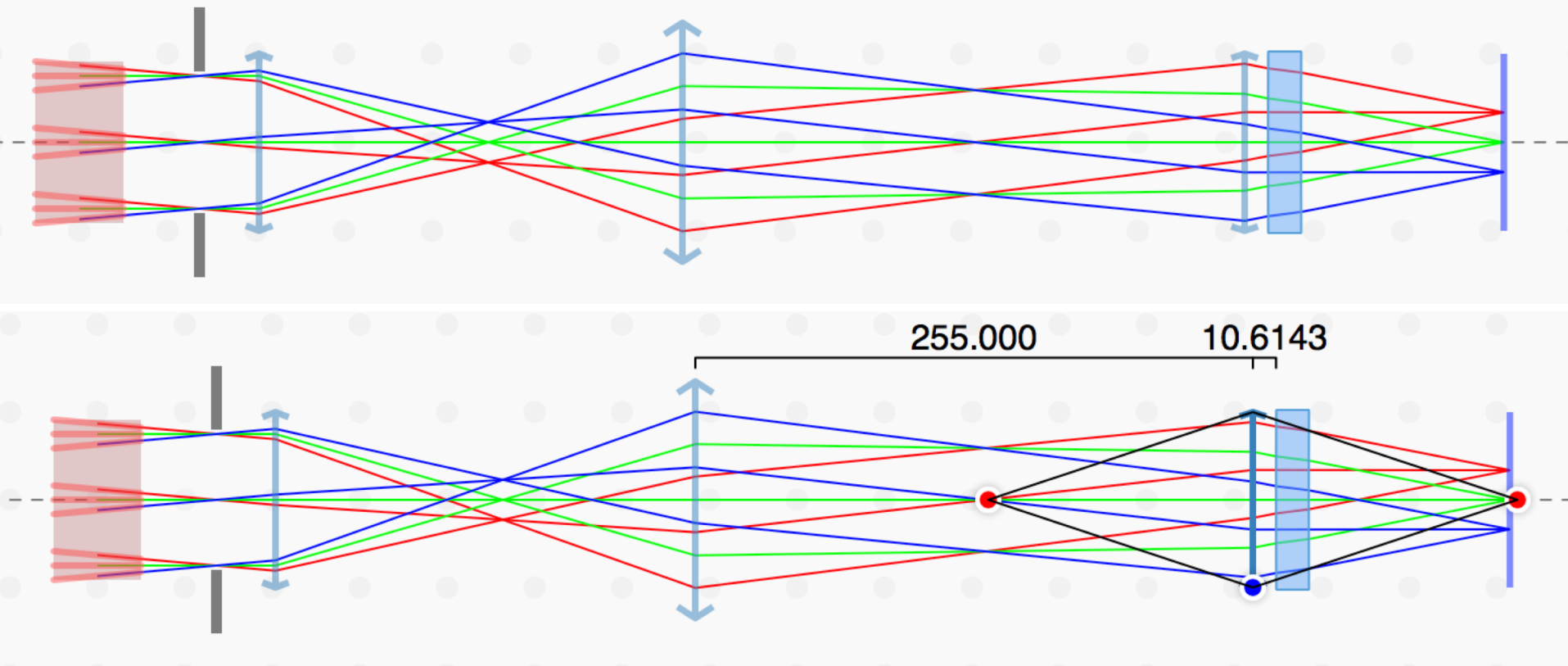
- Filter in image plane, optical quality unimportant
- Rays from different fields pass filter at different angles
- Filter profile will depend on field position
- Cone of rays for each field position broadens filter profile

Example: Interference Filter in Pupil



- Filter in pupil plane, optical quality crucial
- Rays from different fields pass filter at different angles
- Filter profile will depend on field position
- Same incidence angles of all rays from one field position, narrowest possible filter profile

Interference Filter in Telecentric Beam



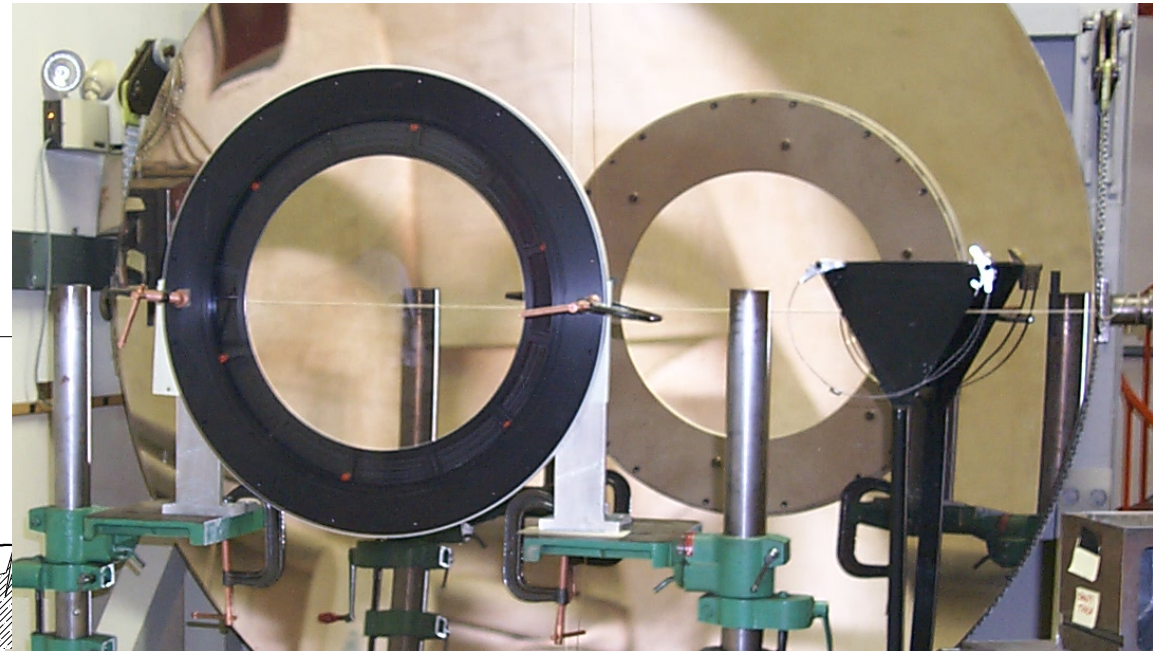
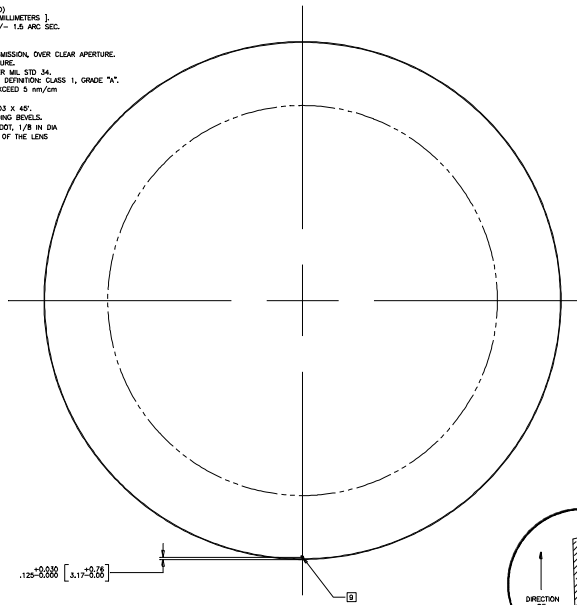
- Last lens is one focal length away from pupil
- Seen from image, pupil is at infinity
- Broadened filter profile, constant across field

Optical Design Principle 8

8. Oversize optical elements

- optical manufacturing quality always worse at edge
- need to hold/mount optical elements
- thermal, stress effects most pronounced at edges

NOTES: UNLESS OTHERWISE NOTED: _____
1. REMOVE ALL BURRS AND SHARP EDGES
2. FINISHED SURFACE ROUGHNESS: $0.25\mu\text{m}$
3. MAT'L: FUSED SILICA (CORNING 7940)
4. DIMENSIONS ARE IN INCHES [AND MILLIMETERS]
5. REQUIRED WEDGE ANGLE TO BE 5.17° - 1.0 ARC SEC.
6. OPTICAL QUALITY:
 = 0.53 rms
 PEAK TO VALLEY = 1° IN TRANSMISSION OVER CLEAR APERTURE.
 RMS = $1/41^\circ$ OVER CLEAR APERTURE.
 SCRATCH AND DIG: 60 - 40 PER MIL STD 54.
 HOMOGENEITY: FOR MIL-G-17478 DEFINITION: CLASS 1, GRADE 7A.
 RESIDUAL STRESS SHALL NOT EXCEED 5 mm/cm
 INCLUSION CLASS 4
7. EDGES SHALL BE BEVELED $.02$ - $.03 \times 45^\circ$.
8. COSMETICALLY POLISH EDGE, INCLUDING BEVELS.
9. INDICATE BY HEAVY OR DOTTING A DOT, $1/8$ IN DIA.
ON WHAT WILL BE THE WEDGE SIDE OF THE LENS
AT LOCATION SHOWN.



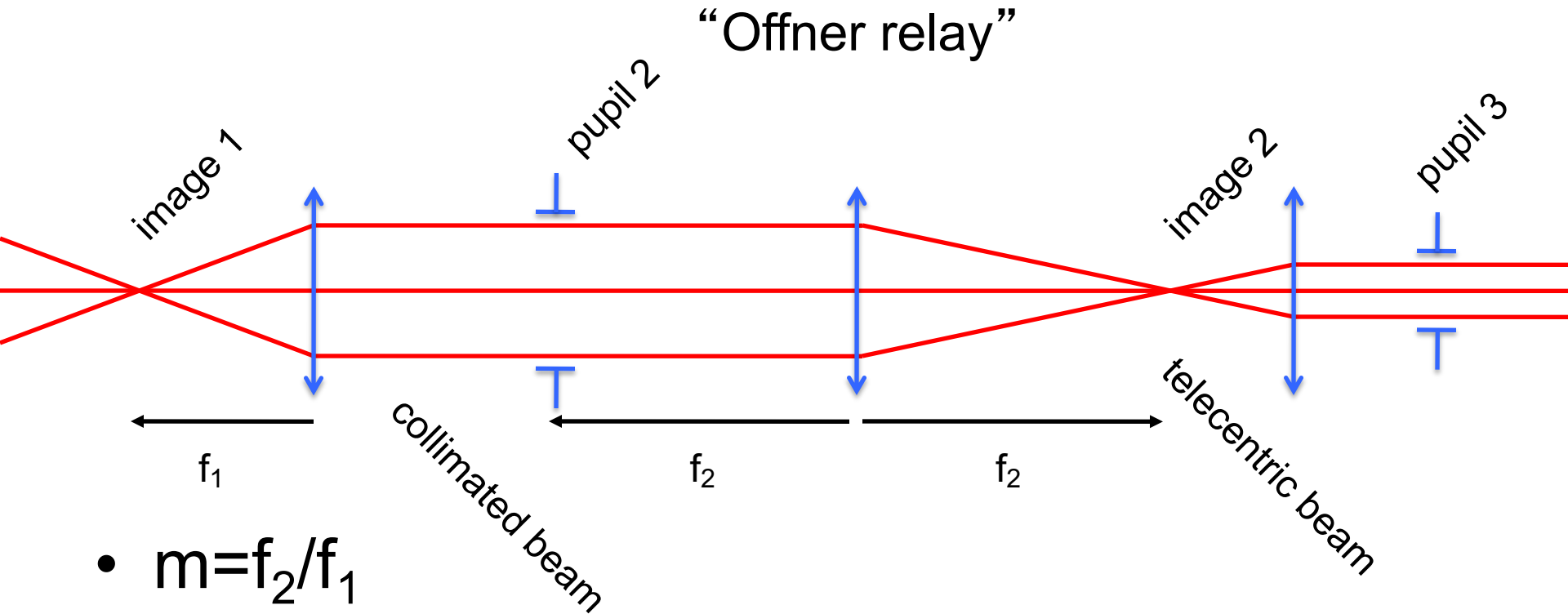
Global Design Choices

- Lenses or mirrors (depends on wavelength range)
- Choice of dispersing elements (prism, grating)
- Location of aperture stop
- Locations of image and pupil planes
- Sampling (Nyquist: >2 pixels per resolution element)
- (dichroic) beam-splitting
- (de-)magnification
- F-numbers; problems $\sim(1/F\text{-number})^{x>1}$
- Operating temperature range, pressure

First-Order Design

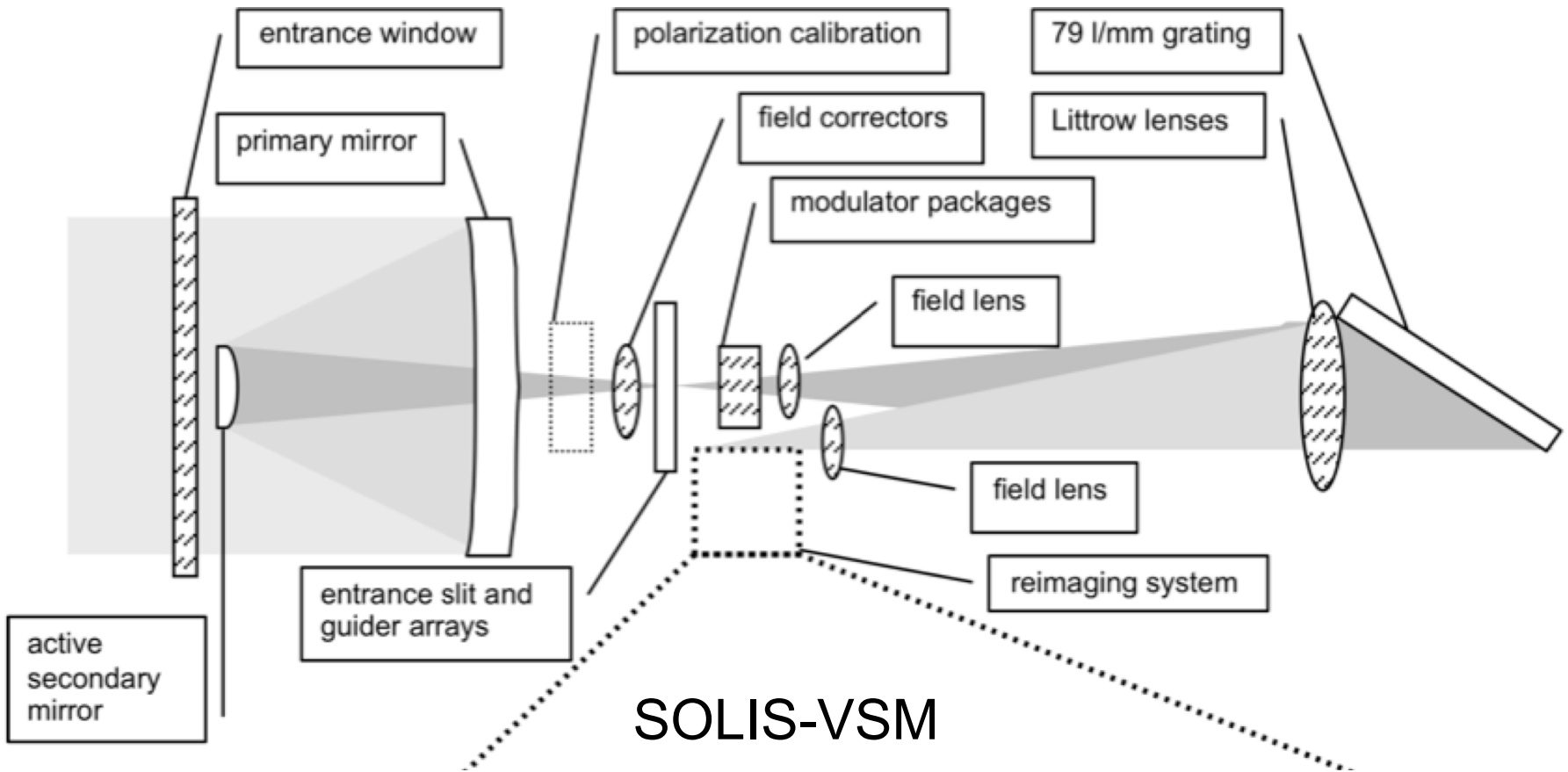
- First-order optical designs use
 - ideal optical elements (e.g. paraxial surfaces)
 - central and extreme field points and rays
 - image and pupil locations
- Establishes general configuration
- Often based on existing designs
- Can be sketched on paper or in a spreadsheet
- Provides first idea of size of different designs

Example First-Order Design 1



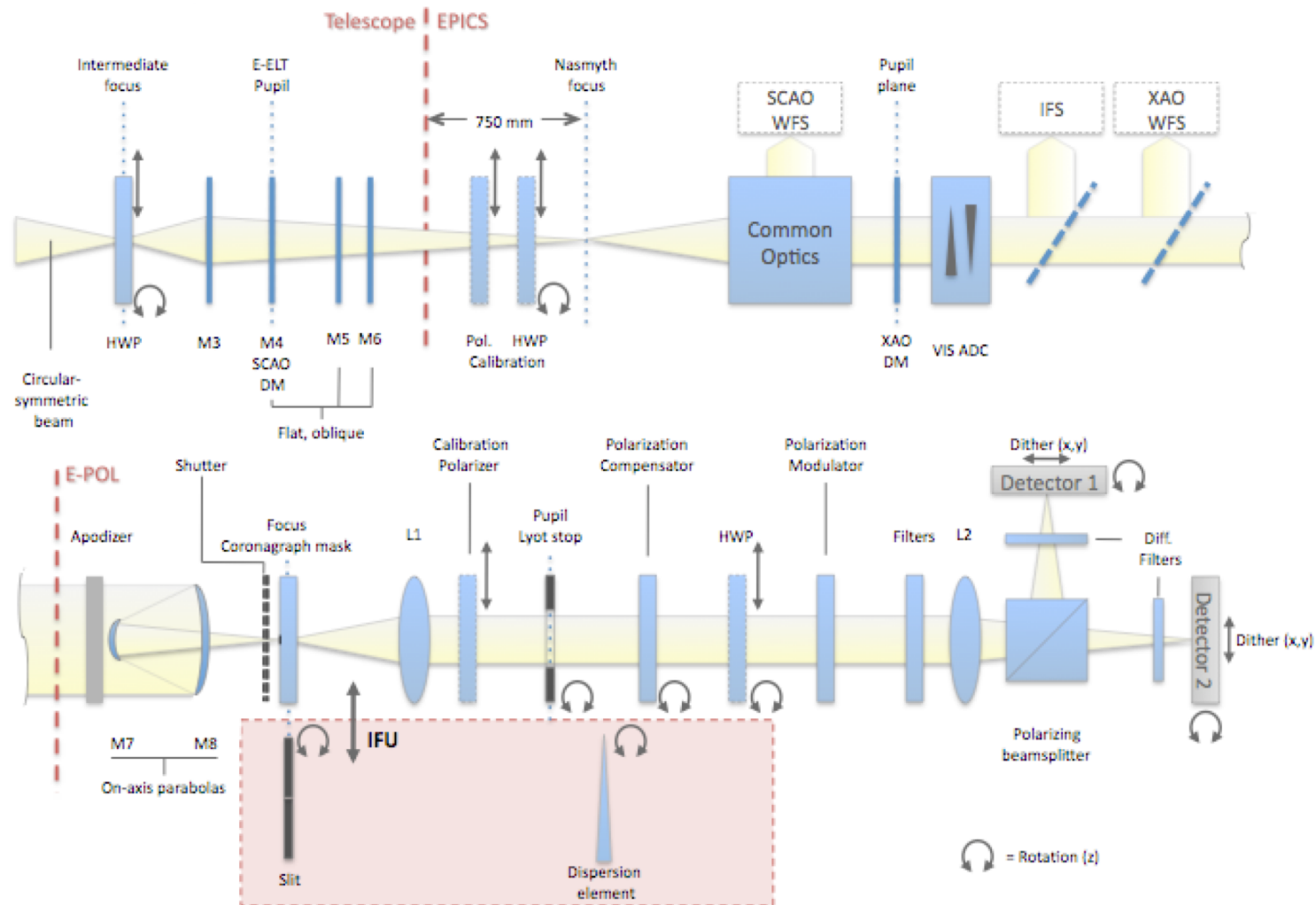
- $m=f_2/f_1$
- minimum geometrical aberrations for symmetric system ($m=1$)

Example First-Order Design 2



First-Order Design Example 3

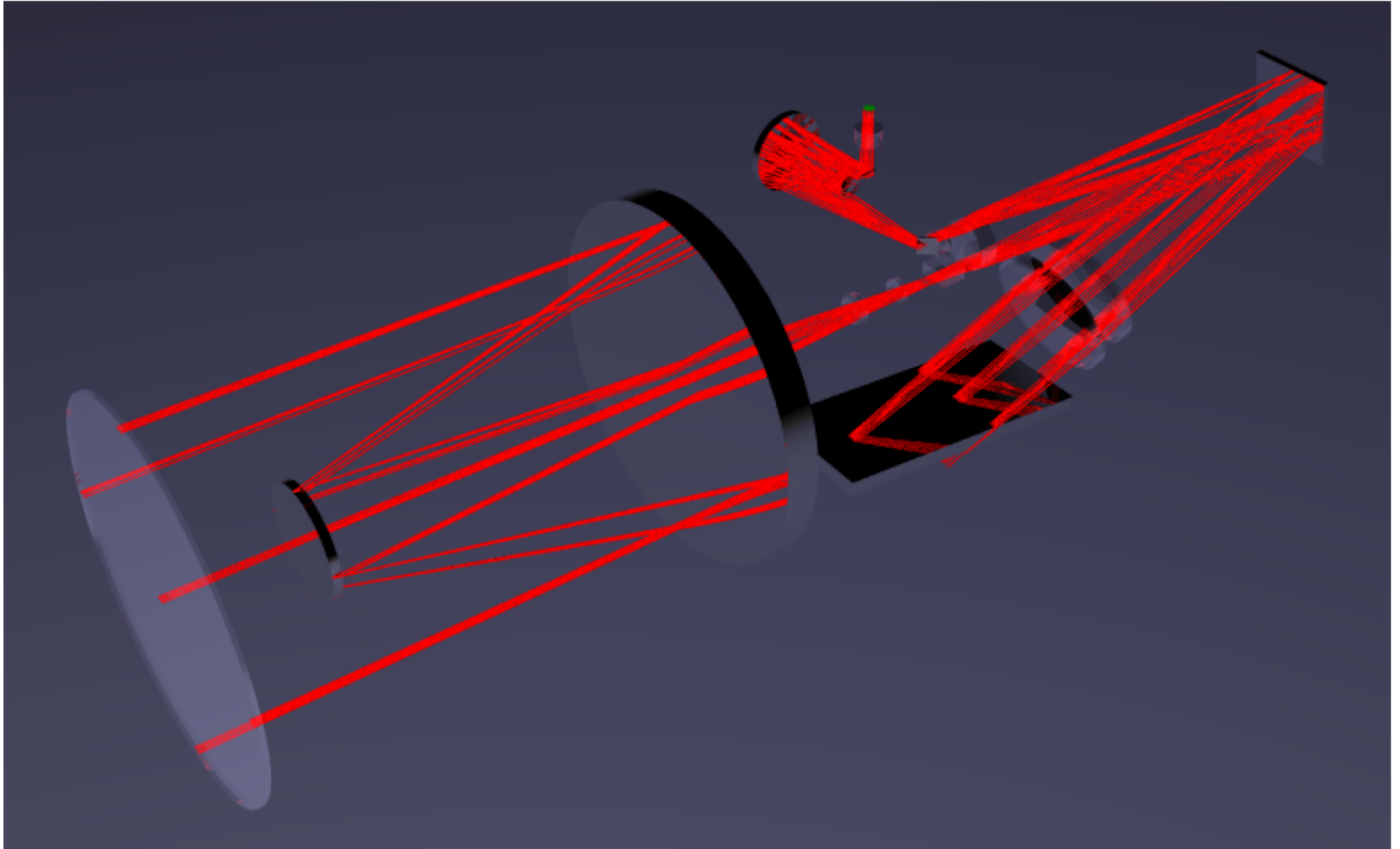
EPICS-EPOL



Ray Tracing

- Ray-tracing based on geometrical optics approximation (wavefronts are locally flat)
- Rays are traced from source to image
- Optical elements are decomposed into surfaces:
 - radius of curvature
 - distance to following surface
 - diameter
 - index of refraction following surface
- Optical design programs: WinLens, ZEMAX, OSLO
- Programs only useful once major design decisions have already been made!

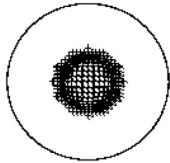
Raytracing Example: SOLIS VSM



Spot Diagrams for Perfect Optics

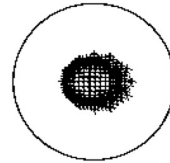
OBJ: 0.0000, 0.0000 DEG

16.00



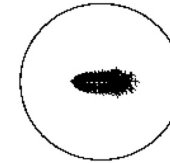
IMA: 0.000, -0.000 MM

OBJ: 0.0930, 0.0000 DEG



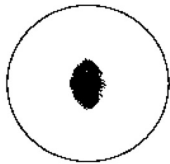
IMA: 5.356, 0.000 MM

OBJ: 0.1870, 0.0000 DEG



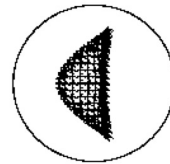
IMA: 10.769, 0.000 MM

OBJ: 0.2800, 0.0000 DEG



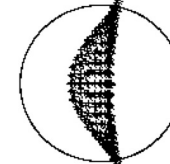
IMA: 16.124, -0.000 MM

OBJ: 0.3700, 0.0000 DEG



IMA: 21.305, -0.000 MM

OBJ: 0.4600, 0.0000 DEG



IMA: 26.489, 0.000 MM

SURFACE: IMA

SPOT DIAGRAM

TELESCOPE, CORRECTOR OPTIMIZATION (TD_SPOT)

MON MAR 29 1999 UNITS ARE MICRONS.

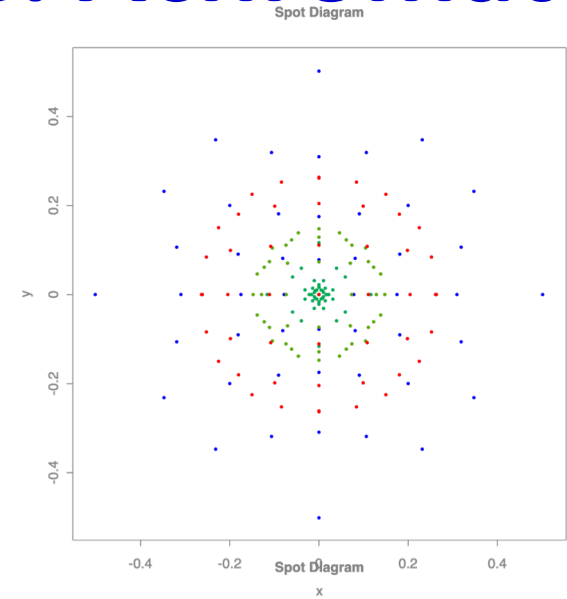
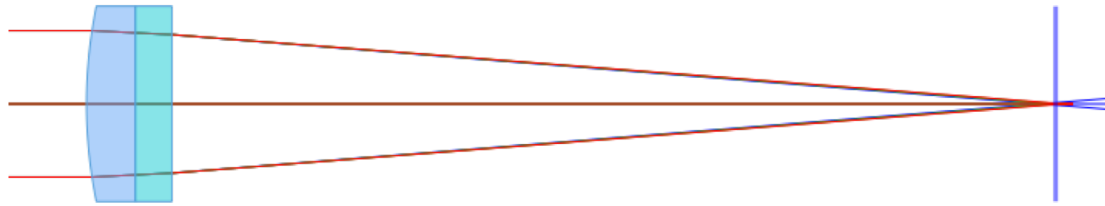
FIELD	1	2	3	4	5	6
RMS RADIUS :	1.641	1.476	0.999	0.790	2.012	2.832
GEO RADIUS :	2.190	2.347	2.131	1.401	3.597	5.503
AIRY DIAM :	10.15					

REFERENCE : CENTROID

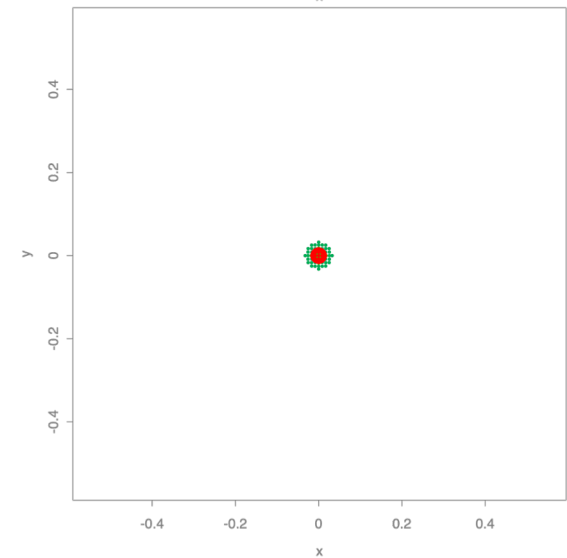
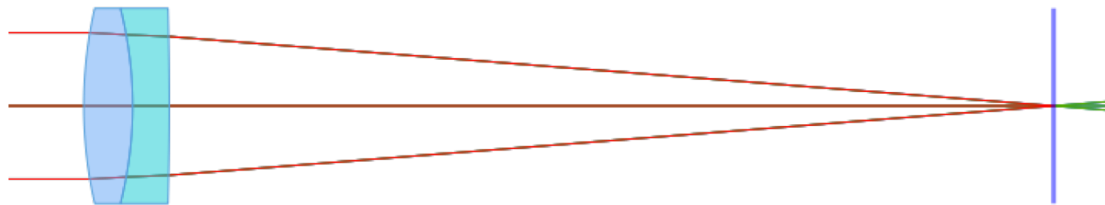
Optimization

- Built into most optical design software
- Automatically improves performance
- Degrees of freedom = variables of optical design
 - radii of curvature of optical surfaces
 - spacing between elements
 - conic constants
 - glass thicknesses
- Can change glass type
- Generally does not add or remove optics
- Must define scalar performance (merit) function

Optimization Example: Achromat



made with Touch Optical Design version 0.40.0 pro



Tolerance Analysis

- Determines tolerances to which
 - optical elements have to be manufactured
 - optical elements have to be positioned
 - environmental parameters have to be controlled
- Often uses optimization merit function to quantify performance change
- Most design parameters are subject to errors
- Compensator parameters are optimized
- Can trade off tolerances between optical elements to optimize manufacturability

Example Monte Carlo Analysis

Monte Carlo Analysis:

Number of trials: 500

Statistics: Normal Distribution

Nominal 0.001782

Best 0.001325

Worst 0.002580

Mean 0.001846

Std Dev 0.000263

Compensator Statistics:

Thickness Surf 57:

Nominal : 12.000000

Minimum : 11.619700

Maximum : 12.364922

Mean : 12.017660

Standard Deviation : 0.126113

98% of Monte Carlo lenses have a merit function below 0.002418.

90% of Monte Carlo lenses have a merit function below 0.002218.

50% of Monte Carlo lenses have a merit function below 0.001829.

10% of Monte Carlo lenses have a merit function below 0.001511.

2% of Monte Carlo lenses have a merit function below 0.001384.

Assuming that we know the manufacturing statistics, Monte Carlo analysis provides likelihood of achieving required performance