

Outline

- 1 Dichroism
- 2 Stress Birefringence
- 3 Electro-Optics

Dichroism in Uniaxial Crystals

- some materials exhibit different absorption properties for orthogonal polarization states (e.g. tourmaline, sheet polarizers)
- for uniaxial crystals can assume complex indices of refraction $\tilde{n}_{x,y,z}$ to describe anisotropic absorption (dichroism)
- choose principal coordinates where both tensors are diagonal
- repeat derivations as before
- Fresnel equation \Rightarrow ratio of electric field components k,l

$$\frac{E_k}{E_l} = \frac{s_k (\tilde{n}^2 - \tilde{\epsilon}_l)}{s_l (\tilde{n}^2 - \tilde{\epsilon}_k)}$$

- same as for non-absorbing materials, but different interpretation
- $\tilde{n}, \tilde{\epsilon}_{l,k}$ complex \Rightarrow ratios are (in general) complex
- ordinary and extraordinary waves are elliptically polarized
- finite conductivity \Rightarrow non-vanishing current density \vec{j}
- displacement vectors not orthogonal to wave vector

Ordinary and Extraordinary Waves in Uniaxial Dichroic Materials

- for uniaxial media with small conductivities, two solutions to Fresnel equation have analogous form

$$\tilde{n}_1^2 = \tilde{n}_o^2, \quad \frac{1}{\tilde{n}_2^2} = \frac{\cos^2 \theta}{\tilde{n}_o^2} + \frac{\sin^2 \theta}{\tilde{n}_e^2}$$

- polarization states of 2 waves almost linear because ratios of electric field components dominated by real parts
- attenuation of ordinary wave independent of wave direction
- attenuation of extraordinary wave depends on angle between wave vector and optic axis θ
- separate equation into real and imaginary parts using $n \gg k$

$$\frac{1}{n_2^2} = \frac{\cos^2 \theta}{n_o^2} + \frac{\sin^2 \theta}{n_e^2}, \quad \frac{k}{n_2^3} = \frac{k_o \cos^2 \theta}{n_o^3} + \frac{k_e \sin^2 \theta}{n_e^3}$$

Extraordinary Wave in Uniaxial Dichroic Materials

- separate equations for real (n) and imaginary (k) parts

$$\frac{1}{n_2^2} = \frac{\cos^2 \theta}{n_o^2} + \frac{\sin^2 \theta}{n_e^2}$$

$$\frac{k}{n_2^3} = \frac{k_o \cos^2 \theta}{n_o^3} + \frac{k_e \sin^2 \theta}{n_e^3}$$

- real part of index obeys same law as for non-absorbing material
- extinction coefficient of extraordinary wave shows similar dependence on angle between wave vector and optic axis
- will understand behavior of sheet polarizers at non-normal incidence with these equations

Stress Birefringence

- mechanical stress induces anisotropy in isotropic material
- stress (force per area) can be external (mechanical mounting, inhomogeneous temperature) or intrinsic (due to manufacturing)
- glass has no fixed melting temperature \Rightarrow stress can be frozen in
- 100 to 1000 hours of *annealing* reduces stress
- refractive indices for polarization parallel and perpendicular to stress

$$n_{\parallel} = n_0 + K_{\parallel}\sigma, \quad n_{\perp} = n_0 + K_{\perp}\sigma$$

- n_0 : index of refraction of unstressed material
- σ : stress
- $K_{\parallel, \perp}$: *stress optical coefficients*
- for polarimetry: interested in birefringence
$$n_{\parallel} - n_{\perp} = (K_{\parallel} - K_{\perp})\sigma = K\sigma$$

Stress Optical Coefficients

typical values for K for different materials

material	stress optical coefficient	thermal expansion coefficient
N-BK7	$2.77 \cdot 10^{-6} \text{ mm}^2/\text{N}$	$8.30 \cdot 10^{-6}/\text{K}$
fused silica	$3.50 \cdot 10^{-6} \text{ mm}^2/\text{N}$	$0.55 \cdot 10^{-6}/\text{K}$
SF57	$0.02 \cdot 10^{-6} \text{ mm}^2/\text{N}$	$9.20 \cdot 10^{-6}/\text{K}$
N-SF57	$2.78 \cdot 10^{-6} \text{ mm}^2/\text{N}$	$9.88 \cdot 10^{-6}/\text{K}$

- K only slightly dependent on wavelength in visible
- intrinsic birefringence
 - $< 2 \text{ nm/cm}$ for the very best glass
 - $< 1 \text{ nm/cm}$ for fused silica
 - 5 nm/cm is typical for precision optics

Introduction

- external fields \Rightarrow isotropic media can become anisotropic
- *electro-optics*: effects of external electric field applied to isotropic media and crystals
- for isotropic crystals (same n for all 3 principal axes)

$$\delta n = n_e - n_o \approx \frac{n^3}{2} (rE + RE^2)$$

- r : Pockels coefficient
- R : Kerr coefficient
- quadratic (Kerr) effect occurs in all crystals, isotropic media
- linear (Pockels) effect only in some crystals

Modification of Dielectric Tensor

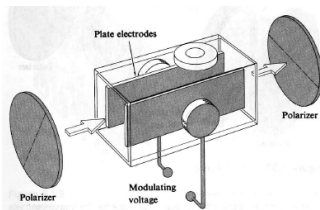
- electric field \Rightarrow change in elements of the inverse dielectric tensor $\left(\frac{1}{\epsilon}\right)_{ij}$
- linear and quadratic electro-optical effects described by tensors

$$\delta \left(\frac{1}{\epsilon}\right)_{ij} = \delta \left(\frac{1}{n^2}\right)_{ij} = r_{ijk} E_k + R_{ijkl} E_k E_l .$$

- many elements of r_{ijk}, R_{ijkl} are zero in crystallographic coordinate system because of symmetries of crystal, non-zero elements are tabulated
- determine new principal axis system in which dielectric tensor is diagonal again
- in piezoelectric crystals (quartz, KDP) and ferroelectric crystals (LiNbO_3), linear effect much larger than quadratic effect
- electro-optical coefficients depend strongly on frequency because of mechanical resonances

Kerr effect

- discovered 1875 by John Kerr in a piece of glass
- also seen in liquids, gases
- isotropic medium becomes uniaxially anisotropic with optic axis parallel to electric field \Rightarrow field perpendicular to line of sight.
- Kerr cells not used much anymore
 - quadratic dependence on electric field strength \Rightarrow very high voltages
 - some of media are toxic or explosive
- birefringence $\Delta n = B\lambda E^2$ with wavelength λ , B Kerr constant

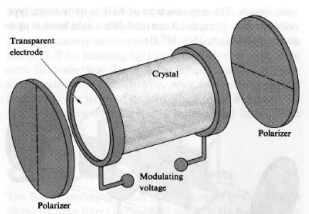


Kerr Constant

Kerr constant, index of refraction for liquids at 550 nm and 22°C

liquid	n	B in 10^{-16} V/m ²
nitrobenzene (C ₆ H ₅ NO ₂)	1.55	44400
acetone (CH ₃ COCH ₃)	1.36	2000
carbon disulfide (CS ₂)	1.63	400
chloroform (CHCl ₃)	1.45	-333

- fast light switches, of the order of a few ps
- effect about one order of magnitude smaller in glasses, often also induced elasto-optical effect due to field-induced deformation.
- effect about 3 orders of magnitude smaller in gasses



- in KDP crystallographic and principal coordinate systems coincide
- electric field along beam, waves polarized at $\pm 45^\circ$ propagate with different speeds
- phase retardation ϕ (units of waves) and voltage V

$$\phi = \frac{n_o^3 r_{63} V}{\lambda}$$

- retardation is independent of distance between electrodes

Pockels Cell Properties

- to minimize field-of-view limitations, distance should be as small as possible
- to minimize sparking, distance should be as large as possible
- depending on needs of application, optimize distance

Crystal Aberrations

Crystal Astigmatism: A converging beam passing a uniaxial, plane-parallel plate is subject to crystal astigmatism. The two focal points along the center ray are separated by

$$\Delta x = \frac{D n_o \sin^2 \Omega (n_e^2 - n_o^2)}{n_e \left(n_o^2 \sin^2 \Omega + n_e^2 \cos^2 \Omega \right)^{\frac{3}{2}}}.$$

Δx Longitudinal astigmatism in units of the plate thickness

D Plate thickness

Ω Angle between optic axis and interface normal

n_o Ordinary index of refraction

n_e Extraordinary index of refraction