# Outline

- **Polarized Light in the Universe**
- <sup>2</sup> Brewster Angle and Total Internal Reflection
- Descriptions of Polarized Light
- <sup>4</sup> Polarizers

# **6** Retarders

## Polarized Light in the Universe

*Polarization* indicates *anisotropy* ⇒ not all directions are equal

Typical anisotropies introduced by

- **e** geometry (not everything is spherically symmetric)
- **•** temperature gradients
- **o** magnetic fields
- electrical fields

# Polarized Light from the Big Bang

- Cosmic Microwave Background (CMB) is red-shifted radiation from Big Bang  $14 \times 10^9$  years ago
- age, geometry, density, of universe from CMB intensity pattern
- **.** first 0.1 seconds from polarization pattern of CMB
- inflation  $\Rightarrow$  gravitational waves  $\Rightarrow$  polarization signals
- polarization expected at (or below)  $10^{-6}$  of intensity

# 13.7 billion year old temperature fluctuations from WMAP



# Unified Model of Active Galactic Nuclei





## Protoplanetary Disk in Scattered Light

## ExPo observation of AB Aurigae  $@$  WHT - 825nm filter



# Solar Magnetic Field Maps from Longitudinal Zeeman Effect



# Planetary Scattered Light



- solar-system planets show scattering polarization
- much depends on cloud height
- can be used to study exoplanets
- ExPo and EPICS developments at UU

## Polarization

- $P$ lane Vector Wave ansatz  $\vec{E} = \vec{E}_0 e^{i(\vec{k} \cdot \vec{x} \omega t)}$
- spatially, temporally constant vector  $\vec{E}_0$  <u>l</u>ays in plane perpendicular to propagation direction  $\vec{k}$
- represent  $\vec{E}_0$  in 2-D basis, unit vectors  $\vec{e}_1$  and  $\vec{e}_2$ , both perpendicular to  $$

$$
\vec{E}_0=E_1\vec{e}_1+E_2\vec{e}_2.
$$

*E*<sub>1</sub>, *E*<sub>2</sub>: arbitrary complex scalars

- damped plane-wave solution with given  $\omega, \, \vec{k}$  has 4 degrees of freedom (two complex scalars)
- additional property is called *polarization*
- many ways to represent these four quantities
- if  $E_1$  and  $E_2$  have identical phases,  $\vec{E}$  oscillates in fixed plane

## Summary of Fresnel Equations

 $\bullet$  electric field amplitude transmission  $t_{s,p}$ , reflection  $r_{s,p}$ 

$$
t_{s} = \frac{2\tilde{n}_{1}\cos\theta_{i}}{\tilde{n}_{1}\cos\theta_{i} + \sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}
$$
\n
$$
t_{p} = \frac{2\tilde{n}_{1}\tilde{n}_{2}\cos\theta_{i}}{\tilde{n}_{2}^{2}\cos\theta_{i} + \tilde{n}_{1}\sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}
$$
\n
$$
r_{s} = \frac{\tilde{n}_{1}\cos\theta_{i} - \sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}{\tilde{n}_{1}\cos\theta_{i} + \sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}
$$
\n
$$
r_{p} = \frac{\tilde{n}_{2}^{2}\cos\theta_{i} - \tilde{n}_{1}\sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}{\tilde{n}_{2}^{2}\cos\theta_{i} + \tilde{n}_{1}\sqrt{\tilde{n}_{2}^{2} - \tilde{n}_{1}^{2}\sin^{2}\theta_{i}}}
$$

reflectivity:  $R = |r_{s,p}|^2$ , transmissivity:  $\mathcal{T} = \frac{|\tilde{n}_2|\cos\theta_i}{|\tilde{n}_1|\cos\theta_i}$  $\frac{|\tilde{n}_2|\cos\theta_t}{|\tilde{n}_1|\cos\theta_i}\,|t_{\mathcal{S},\mathcal{P}}|^2$ 

#### Brewster Angle



• 
$$
r_p = \frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)} = 0
$$
 when  $\theta_i + \theta_t = \frac{\pi}{2}$ 

- corresponds to *Brewster angle* of incidence of tan  $\theta_B = \frac{n_2}{n_1}$ *n*1
- occurs when reflected wave is perpendicular to transmitted wave
- reflected light is completely s-polarized
- **•** transmitted light is moderately polarized

# Total Internal Reflection (TIR)



• Snell's law: 
$$
\sin \theta_t = \frac{n_1}{n_2} \sin \theta_i
$$

- wave from high-index medium into lower index medium (e.g. glass to air):  $n_1/n_2 > 1$
- right-hand side  $> 1$  for sin  $\theta_i > \frac{n_2}{n_1}$ *n*1
- all light is reflected in high-index medium ⇒ *total internal reflection*
- $\bullet$  transmitted wave has complex phase angle  $\Rightarrow$  damped wave along interface

# Phase Change on Total Internal Reflection (TIR)

- TIR induces phase change that depends on polarization
- **o** complex ratios:
	- $r_{\mathcal{S},\rho}=|r_{\mathcal{S},\rho}|e^{i\delta_{\mathcal{S},\rho}}$
- **o** phase change  $\delta = \delta_s \delta_p$

$$
\tan\frac{\delta}{2}=\frac{\cos\theta_i\sqrt{\sin^2\theta_i-\left(\frac{n_2}{n_1}\right)^2}}{\sin^2\theta_i}
$$

- **•** relation valid between critical angle and grazing incidence
- for critical angle and grazing incidence, phase difference is zero



# Polarization Ellipse



- $\vec{E}$  (*t*) =  $\vec{E}_0 e^{i(\vec{k}\cdot\vec{x}-\omega t)}$  $\vec{E}_0 = E_1 e^{i\delta_1} \vec{e}_x + E_2 e^{i\delta_2} \vec{e}_y$ wave vector in *z*-direction •  $\vec{e}_x$ ,  $\vec{e}_y$ : unit vectors in *x*, *y*
- $\bullet$  *E*<sub>1</sub>, *E*<sub>2</sub>: (real) amplitudes
- $\bullet$   $\delta_{1,2}$ : (real) phases

# Polarization Description

- 2 complex scalars not the most useful description
- at given  $\vec{x}$ , time evolution of  $\vec{E}$  described by *polarization ellipse*
- **e** ellipse described by axes *a*, *b*, orientation  $\psi$



# Jones Formalism

#### Jones Vectors

$$
\vec{E}_0 = E_x \vec{e}_x + E_y \vec{e}_y
$$

- **o** beam in z-direction
- $\vec{e}_x$ ,  $\vec{e}_y$  unit vectors in *x*, *y*-direction
- $\bullet$  complex scalars  $E_{X,Y}$
- Jones vector

$$
\vec{e} = \left(\begin{array}{c} E_x \\ E_y \end{array}\right)
$$

- **•** phase difference between  $E_x$ ,  $E_y$  multiple of  $\pi$ , electric field vector oscillates in a fixed plane ⇒ *linear polarization*
- phase difference  $\pm \frac{\pi}{2} \Rightarrow$  *circular polarization*

#### Summing and Measuring Jones Vectors

$$
\vec{E}_0 = E_x \vec{e}_x + E_y \vec{e}_y
$$

$$
\vec{e} = \begin{pmatrix} E_x \\ E_y \end{pmatrix}
$$

- Maxwell's equations linear  $\Rightarrow$  sum of two solutions again a solution
- $\bullet$  Jones vector of sum of two waves  $=$  sum of Jones vectors of individual waves if wave vectors  $\vec{k}$  the same
- **•** addition of Jones vectors: *coherent* superposition of waves
- elements of Jones vectors are not observed directly
- observables always depend on products of elements of Jones vectors, i.e. intensity

$$
I = \vec{e} \cdot \vec{e}^* = e_x e_x^* + e_y e_y^*
$$

#### Jones matrices

• influence of medium on polarization described by  $2 \times 2$  complex *Jones matrix* J

$$
\vec{e}' = J\vec{e} = \left(\begin{array}{cc} J_{11} & J_{12} \\ J_{21} & J_{22} \end{array}\right)\vec{e}
$$

- assumes that medium not affected by polarization state
- different media 1 to *N* in order of wave direction ⇒ combined influence described by

$$
J=J_NJ_{N-1}\cdots J_2J_1
$$

- order of matrices in product is crucial
- Jones calculus describes coherent superposition of polarized light

Linear Polarization	Cii
o horizontal: $\begin{pmatrix} 1 \\ 0 \end{pmatrix}$	
o vertical: $\begin{pmatrix} 0 \\ 1 \end{pmatrix}$	
o 45°: $\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$	

Circular Polarization

\n\n- left: 
$$
\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}
$$
\n- right:  $\frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -i \end{pmatrix}$
\n

# Notes on Jones Formalism

- Jones formalism operates on amplitudes, not intensities
- coherent superposition important for coherent light (lasers, interference effects)
- **.** Jones formalism describes 100% polarized light

# Stokes and Mueller Formalisms

# Stokes Vector

- **•** formalism to describe polarization of quasi-monochromatic light
- **•** directly related to measurable intensities
- Stokes vector fulfills these requirements

$$
\vec{l} = \left(\begin{array}{c} l \\ Q \\ U \\ V \end{array}\right) = \left(\begin{array}{c} E_x E_x^* + E_y E_y^* \\ E_x E_x^* - E_y E_y^* \\ E_x E_y^* + E_y E_x^* \\ i \left(E_x E_y^* - E_y E_x^*\right) \end{array}\right) = \left(\begin{array}{c} E_1^2 + E_2^2 \\ E_1^2 - E_2^2 \\ 2E_1 E_2 \cos \delta \\ 2E_1 E_2 \sin \delta \end{array}\right)
$$

Jones vector elements  $E_{x,y}$ , real amplitudes  $E_{1,2}$ , phase difference  $\delta = \delta_2 - \delta_1$ 

• 
$$
I^2 \ge Q^2 + U^2 + V^2
$$

• can describe unpolarized  $(Q = U = V = 0)$  light





# Stokes Vector Interpretation

$$
\vec{l} = \begin{pmatrix} l \\ Q \\ U \\ V \end{pmatrix} = \begin{pmatrix} intensity \\ linear 0^{\circ} - linear 90^{\circ} \\ linear 45^{\circ} - linear 135^{\circ} \\ circular left - right \end{pmatrix}
$$

*degree of polarization*

$$
P=\frac{\sqrt{Q^2+U^2+V^2}}{I}
$$

1 for fully polarized light, 0 for unpolarized light

summing of Stokes vectors = *incoherent* adding of quasi-monochromatic light waves





# Mueller Matrices

 $\bullet$  4  $\times$  4 real Mueller matrices describe (linear) transformation between Stokes vectors when passing through or reflecting from media

$$
\vec{I}'=M\vec{I}\,,
$$

$$
M = \left(\begin{array}{cccc} M_{11} & M_{12} & M_{13} & M_{14} \\ M_{21} & M_{22} & M_{23} & M_{24} \\ M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{array}\right)
$$

• *N* optical elements, combined Mueller matrix is

$$
M'=M_{\textstyle\mathcal N} M_{\textstyle\mathcal N-1}\cdots M_2 M_1
$$

# Rotating Mueller Matrices

- optical element with Mueller matrix M
- Mueller matrix of the same element rotated by  $\theta$  around the beam given by

$$
M(\theta) = R(-\theta)MR(\theta)
$$

with

$$
R(\theta) = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2\theta & \sin 2\theta & 0 \\ 0 & -\sin 2\theta & \cos 2\theta & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}
$$

Vertical Linear Polarizer

$$
M_{pol}(\theta) = \frac{1}{2} \begin{pmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}
$$

Horizontal Linear Polarizer

$$
M_{pol}\left(\theta\right)=\frac{1}{2}\left(\begin{array}{cccc}1&-1&0&0\\-1&1&0&0\\0&0&0&0\\0&0&0&0\end{array}\right)
$$

Mueller Matrix for Ideal Linear Polarizer at Angle  $\theta$ 

$$
\mathsf{M}_{pol}\left(\theta\right)=\frac{1}{2}\left(\begin{array}{ccc}1&\cos2\theta&\sin2\theta&0\\ \cos2\theta&\cos^{2}2\theta&\sin2\theta\cos2\theta&0\\ \sin2\theta&\sin2\theta\cos2\theta&\sin^{2}2\theta&0\\ 0&0&0&0\end{array}\right)
$$

# Poincaré Sphere



#### Relation to Stokes Vector

- **•** fully polarized light:  $I^2 = Q^2 + U^2 + V^2$
- for *I* <sup>2</sup> = 1: sphere in *Q*, *U*, *V* coordinate system
- **o** point on Poincaré sphere represents particular state of polarization
- graphical representation of fully polarized light



- **•** polarizer: optical element that produces polarized light from unpolarized input light
- **.** linear, circular, or in general elliptical polarizer, depending on type of transmitted polarization
- **•** linear polarizers by far the most common
- large variety of polarizers

#### Jones Matrix for Linear Polarizers

• Jones matrix for linear polarizer:

$$
J_{\rho}=\left(\begin{array}{cc}\rho_x & 0 \\ 0 & \rho_y\end{array}\right)
$$

 $\bullet$  0  $\leq$   $p_x \leq$  1 and 0  $\leq$   $p_y \leq$  1, real: transmission factors for *x*, *y*-components of electric field:  $E'_x = p_x E_x$ ,  $E'_y = p_y E_y$ 

- $p_x = 1$ ,  $p_y = 0$ : linear polarizer in  $+Q$  direction
- $p_x = 0$ ,  $p_y = 1$ : linear polarizer in  $-Q$  direction
- $p_x = p_y$ : neutral density filter

#### Mueller Matrix for Linear Polarizers

$$
M_p = \frac{1}{2} \left( \begin{array}{rrrr} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{array} \right)
$$

# Mueller Matrix for Ideal Linear Polarizer at Angle  $\theta$



# Poincare Sphere



- polarizer is a point on the Poincaré sphere
- transmitted intensity: cos<sup>2</sup>(//2), *l* is arch length of great circle between incoming polarization and polarizer on Poincaré sphere

#### Wire Grid Polarizers





- **•** parallel conducting wires, spacing  $d \leq \lambda$  act as polarizer
- **e** electric field parallel to wires induces electrical currents in wires
- induced electrical current reflects polarization parallel to wires
- polarization perpendicular to wires is transmitted
- rule of thumb:
	- $d < \lambda/2$   $\Rightarrow$  strong polarization
	- $d \gg \lambda \Rightarrow$  high transmission of both polarization states (weak polarization)
- mostly used in infrared

# Polaroid-type Polarizers



- developed by Edwin Land in 1938  $\Rightarrow$  Polaroid
- sheet polarizers: stretched polyvynil alcohol (PVA) sheet, laminated to sheet of cellulose acetate butyrate, treated with iodine
- PVA-iodine complex analogous to short, conducting wire
- cheap, can be manufactured in large sizes

#### Crystal-Based Polarizers



- **•** crystals are basis of highest-quality polarizers
- precise arrangement of atom/molecules and anisotropy of index of refraction separate incoming beam into two beams with precisely orthogonal linear polarization states
- work well over large wavelength range
- many different configurations
- **o** calcite most often used in crystal-based polarizers because of large birefringence, low absorption in visible
- many other suitable materials

#### Retarders or Wave Plates



- **•** retards (delays) phase of one electric field component with respect to orthogonal component
- **•** anisotropic material (crystal) has index of refraction that depends on polarization

## Retarder Properties

- **o** does not change intensity or degree of polarization
- **•** characterized by two (not identical, not trivial) Stokes vectors of incoming light that are not changed by retarder ⇒ *eigenvectors* of retarder
- **•** depending on polarization described by eigenvectors, retarder is
	- *linear retarder*
	- *circular retarder*
	- *elliptical retarder*
- **.** linear, circular retarders are special cases of elliptical retarders
- circular retarders sometimes called *rotators* since they rotate the orientation of linearly polarized light
- **.** linear retarders by far the most common type of retarder

#### Jones Matrix for Linear Retarders

• linear retarder with fast axis at  $0^\circ$  characterized by Jones matrix

$$
J_r(\delta)=\left(\begin{array}{cc}e^{i\delta}&0\\0&1\end{array}\right),\quad J_r(\delta)=\left(\begin{array}{cc}e^{i\frac{\delta}{2}}&0\\0&e^{-i\frac{\delta}{2}}\end{array}\right)
$$

- $\bullet$   $\delta$ : phase shift between two linear polarization components (in radians)
- absolute phase does not matter

#### Mueller Matrix for Linear Retarder

$$
M_r=\left(\begin{array}{cccc}1&0&0&0\\0&1&0&0\\0&0&\cos\delta&-\sin\delta\\0&0&\sin\delta&\cos\delta\end{array}\right)
$$

## Quarter-Wave Plate on the Poincaré Sphere



- retarder eigenvector (fast axis) in Poincaré sphere  $\bullet$
- points on sphere are rotated around retarder axis by amount of retardation

#### Variable Retarders

- **•** sensitive polarimeters requires retarders whose properties (retardance, fast axis orientation) can be varied quickly (*modulated*)
- **•** retardance changes (change of birefringence):
	- liquid crystals
	- Faraday, Kerr, Pockels cells
	- piezo-elastic modulators (PEM)
- fast axis orientation changes (change of *c*-axis direction):
	- rotating fixed retarder
	- ferro-electric liquid crystals (FLC)

# Liquid Crystals



- **•** liquid crystals: fluids with elongated molecules
- **•** at high temperatures: liquid crystal is isotropic
- **•** at lower temperature: molecules become ordered in orientation and sometimes also space in one or more dimensions
- **•** liquid crystals can line up parallel or perpendicular to external electrical field

## Liquid Crystal Retarders



- $\bullet$  dielectric constant anisotropy often large  $\Rightarrow$  very responsive to changes in applied electric field
- birefringence δ*n* can be very large (larger than typical crystal birefringence)
- liquid crystal layer only a few  $\mu$ m thick
- **•** birefringence shows strong temperature dependence