Outline

1. Electromagnetic Waves
2. Material Properties
3. Electromagnetic Waves Across Interfaces
4. Fresnel Equations
5. Brewster Angle
6. Total Internal Reflection

Electromagnetic Waves

Electromagnetic Waves in Matter

- *Maxwell's equations* $\Rightarrow$ electromagnetic waves
- optics: interaction of electromagnetic waves with matter as described by *material equations*
- polarization of electromagnetic waves are integral part of optics

Maxwell's Equations in Matter

$$\nabla \cdot \vec{D} = 4\pi\rho$$

$$\nabla \times \vec{H} - \frac{1}{c}\frac{\partial \vec{D}}{\partial t} = \frac{4\pi}{c}\vec{j}$$

$$\nabla \times \vec{E} + \frac{1}{c}\frac{\partial \vec{B}}{\partial t} = 0$$

$$\nabla \cdot \vec{B} = 0$$

Symbols

$\vec{D}$ *electric displacement*
ρ *electric charge density*
$\vec{H}$ *magnetic field*
c *speed of light in vacuum*
$\vec{j}$ *electric current density*
$\vec{E}$ *electric field*
$\vec{B}$ *magnetic induction*
t time

Linear Material Equations

$$\vec{D} = \epsilon \vec{E}$$
$$\vec{B} = \mu \vec{H}$$
$$\vec{j} = \sigma \vec{E}$$

Symbols

- ϵ *dielectric constant*
- μ *magnetic permeability*
- σ *electrical conductivity*

Isotropic and Anisotropic Media

- isotropic media: ϵ and μ are scalars
- anisotropic media: ϵ and μ are tensors of rank 2
- isotropy of medium broken by
  - anisotropy of material itself (e.g. crystals)
  - external fields (e.g. Kerr effect)

Wave Equation in Matter

- static, homogeneous medium with no net charges: $\rho = 0$
- for most materials: $\mu = 1$
- combine Maxwell, material equations $\Rightarrow$ differential equations for damped (vector) wave

$$\nabla^2 \vec{E} - \frac{\mu\epsilon}{c^2}\frac{\partial^2 \vec{E}}{\partial t^2} - \frac{4\pi\mu\sigma}{c^2}\frac{\partial \vec{E}}{\partial t} = 0$$

$$\nabla^2 \vec{H} - \frac{\mu\epsilon}{c^2}\frac{\partial^2 \vec{H}}{\partial t^2} - \frac{4\pi\mu\sigma}{c^2}\frac{\partial \vec{H}}{\partial t} = 0$$

- damping controlled by conductivity σ
- $\vec{E}$ and $\vec{H}$ are equivalent $\Rightarrow$ sufficient to consider $\vec{E}$
- interaction with matter almost always through $\vec{E}$
- but: at interfaces, boundary conditions for $\vec{H}$ are crucial

Plane-Wave Solutions

- Plane Vector Wave ansatz $\vec{E} = \vec{E}_0 e^{i\left(\vec{k}\cdot\vec{x}-\omega t\right)}$
  - $\vec{k}$ spatially and temporally constant *wave vector*
  - $\vec{k}$ normal to surfaces of constant phase
  - $|\vec{k}|$ *wave number*
  - $\vec{x}$ spatial location
  - ω *angular frequency* ($2\pi\times$ frequency)
  - t time
  - $\vec{E}_0$ (generally complex) vector independent of time and space
- could also use $\vec{E} = \vec{E}_0 e^{-i\left(\vec{k}\cdot\vec{x}-\omega t\right)}$
- damping if $\vec{k}$ is complex
- real electric field vector given by real part of $\vec{E}$

Complex Index of Refraction

- temporal derivatives $\Rightarrow$ Helmholtz equation

$$\nabla^2 \vec{E} + \frac{\omega^2 \mu}{c^2} \left(\epsilon + i \frac{4\pi\sigma}{\omega} \right) \vec{E} = 0$$

- *dispersion relation* between $\vec{k}$ and ω

$$\vec{k} \cdot \vec{k} = \frac{\omega^2 \mu}{c^2} \left(\epsilon + i \frac{4\pi\sigma}{\omega} \right)$$

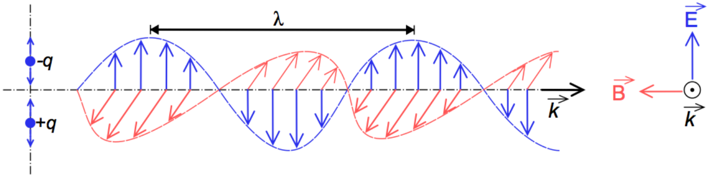
- *complex index of refraction*

$$\tilde{n}^2 = \mu \left(\epsilon + i \frac{4\pi\sigma}{\omega} \right), \quad \vec{k} \cdot \vec{k} = \frac{\omega^2}{c^2} \tilde{n}^2$$

- split into real (n: *index of refraction*) and imaginary parts (k: *extinction coefficient*)

$$\tilde{n} = n + ik$$

Transverse Waves



- plane-wave solution must also fulfill Maxwell's equations

$$\vec{E}_0 \cdot \vec{k} = 0, \quad \vec{H}_0 \cdot \vec{k} = 0, \quad \vec{H}_0 = \frac{\tilde{n}}{\mu} \frac{\vec{k}}{|\vec{k}|} \times \vec{E}_0$$

- isotropic media: electric, magnetic field vectors normal to wave vector $\Rightarrow$ transverse waves
- $\vec{E}_0$, $\vec{H}_0$, and $\vec{k}$ orthogonal to each other, right-handed vector-triple
- conductive medium $\Rightarrow$ complex $\tilde{n}$, $\vec{E}_0$ and $\vec{H}_0$ out of phase
- $\vec{E}_0$ and $\vec{H}_0$ have constant relationship $\Rightarrow$ consider only $\vec{E}$

Energy Propagation in Isotropic Media

- *Poynting vector*

$$\vec{S} = \frac{c}{4\pi}\left(\vec{E} \times \vec{H}\right)$$

- $|\vec{S}|$: energy through unit area perpendicular to $\vec{S}$ per unit time
- direction of $\vec{S}$ is direction of energy flow
- time-averaged Poynting vector given by

$$\left\langle \vec{S} \right\rangle = \frac{c}{8\pi} \mathrm{Re}\left(\vec{E}_0 \times \vec{H}_0^*\right)$$

Re	real part of complex expression
*	complex conjugate
$\langle . \rangle$	time average

- energy flow parallel to wave vector (in isotropic media)

$$\left\langle \vec{S} \right\rangle = \frac{c}{8\pi} \frac{|\tilde{n}|}{\mu} \left|E_0\right|^2 \frac{\vec{k}}{|\vec{k}|}$$

Quasi-Monochromatic Light

- monochromatic light: purely theoretical concept
- monochromatic light wave always fully polarized
- real life: light includes range of wavelengths $\Rightarrow$ *quasi-monochromatic light*
- quasi-monochromatic: superposition of mutually incoherent monochromatic light beams whose wavelengths vary in narrow range $\delta\lambda$ around central wavelength λ_0

$$\frac{\delta\lambda}{\lambda} \ll 1$$

- measurement of quasi-monochromatic light: integral over measurement time t_m
- amplitude, phase (slow) functions of time for given spatial location
- *slow*: variations occur on time scales much longer than the mean period of the wave

Polarization of Quasi-Monochromatic Light

- electric field vector for quasi-monochromatic plane wave is sum of electric field vectors of all monochromatic beams

$$\vec{E}\,(t) = \vec{E}_0\,(t)\,e^{i\left(\vec{k}\cdot\vec{x}-\omega t\right)}$$

- can write this way because $\delta\lambda \ll \lambda_0$
- measured intensity of quasi-monochromatic beam

$$\left\langle \vec{E}_x \vec{E}_x^* \right\rangle + \left\langle \vec{E}_y \vec{E}_y^* \right\rangle = \lim_{t_m -> \infty} \frac{1}{t_m} \int_{-t_m/2}^{t_m/2} \vec{E}_x(t)\vec{E}_x^*(t) + \vec{E}_y(t)\vec{E}_y^*(t) dt$$

$\langle \cdots \rangle$: averaging over measurement time t_m

- measured intensity independent of time
- quasi-monochromatic: frequency-dependent material properties (e.g. index of refraction) are constant within $\Delta\lambda$

Polychromatic Light or White Light

- wavelength range comparable wavelength ($\frac{\delta\lambda}{\lambda} \sim 1$)
- incoherent sum of quasi-monochromatic beams that have large variations in wavelength
- cannot write electric field vector in a plane-wave form
- must take into account frequency-dependent material characteristics
- intensity of polychromatic light is given by sum of intensities of constituting quasi-monochromatic beams

Material Properties

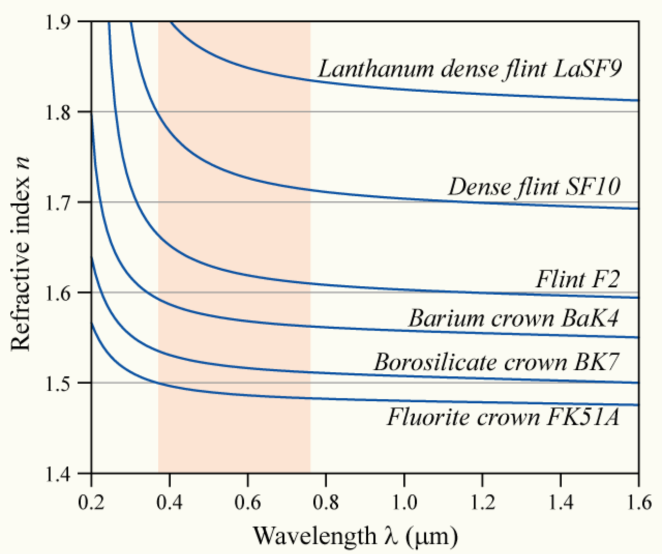
Index of Refraction

- complex index of refraction

$$\tilde{n}^2 = \mu \left(\epsilon + i \frac{4\pi\sigma}{\omega} \right), \quad \vec{k} \cdot \vec{k} = \frac{\omega^2}{c^2} \tilde{n}^2$$

- no electrical conductivity $\Rightarrow$ real index of refraction
- dielectric materials: real index of refraction
- conducting materials (metal): complex index of refraction
- index of refraction depends on wavelength (dispersion)
- index of refraction depends on temperature
- index of refraction roughly proportional to density

Glass Dispersion



http://en.wikipedia.org/wiki/File:Dispersion-curve.png

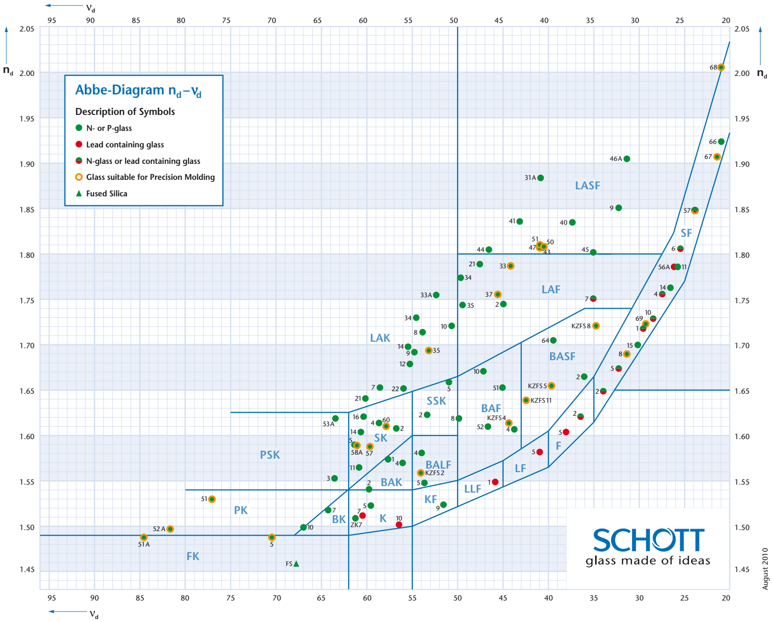
Wavelength Dependence of Index of Refraction

- tabulated by glass manufacturer
- various approximations to express wavelength dependence with a few parameters
- typically index increases with decreasing wavelength
- Abbé number:

$$\nu_d = \frac{n_d - 1}{n_F - n_C}$$

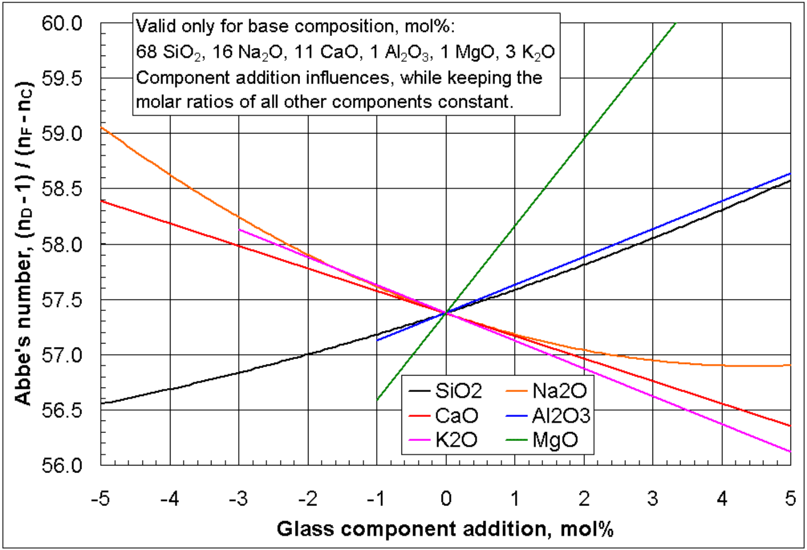
- n_d: index of refraction at Fraunhofer d line (587.6 nm)
- n_F: index of refraction at Fraunhofer F line (486.1 nm)
- n_C: index of refraction at Fraunhofer C line (656.3 nm)
- low dispersion materials have high values of ν_d
- Abbe diagram: ν_d vs n_d

Glasses



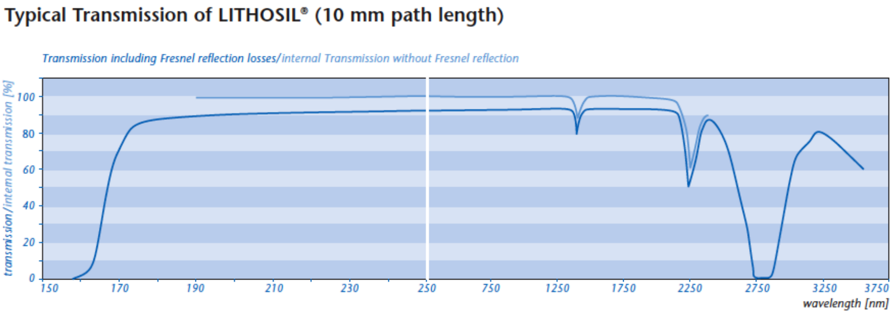
Abbe-Diagram $n_d - \nu_d$
Description of Symbols
N- or P-glass
Lead containing glass
N-glass or lead containing glass
Glass suitable for Precision Molding
Fused Silica
ν_d
n_d
LASF
LAF
SF
LAK
BASF
SSK
BAF
SK
PSK
BALF
F
LF
BAK
LLF
KF
PK
BK
K
FK
SCHOTT
glass made of ideas
August 2010

Glass Ingredients



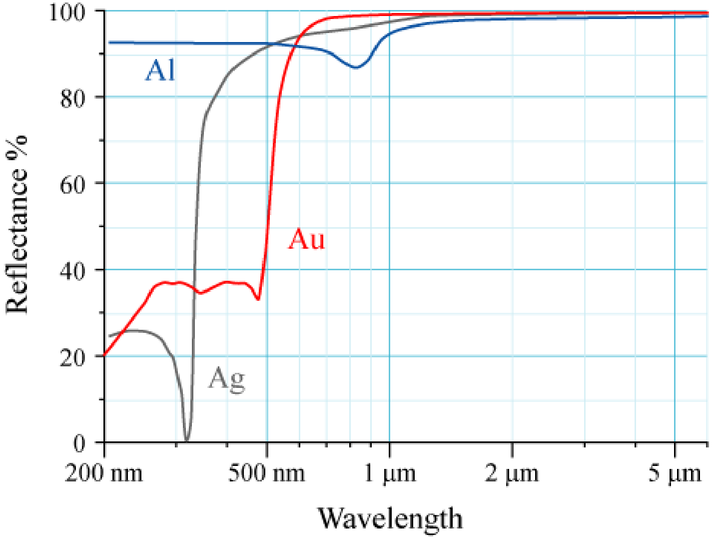
http://glassproperties.com/abbe_number

Internal Transmission



- internal transmission per cm
- typically strong absorption in the blue and UV
- almost all glass absorbs above 2 μm

Metal Reflectivity



http://commons.wikimedia.org/wiki/File:Image-Metal-reflectance.png

Introduction

- classical optics due to interfaces between 2 different media
- from Maxwell's equations in integral form at interface from medium 1 to medium 2

$$
\begin{aligned}
\left(\vec{D}_2 - \vec{D}_1\right) \cdot \vec{n} &= 4\pi\Sigma \\
\left(\vec{B}_2 - \vec{B}_1\right) \cdot \vec{n} &= 0 \\
\left(\vec{E}_2 - \vec{E}_1\right) \times \vec{n} &= 0 \\
\left(\vec{H}_2 - \vec{H}_1\right) \times \vec{n} &= -\frac{4\pi}{c}\vec{K}
\end{aligned}
$$

$\vec{n}$ normal on interface, points from medium 1 to medium 2
Σ surface charge density on interface
$\vec{K}$ surface current density on interface

Fields at Interfaces

- $\Sigma = 0$ in general, $\vec{K} = 0$ for dielectrics
- *complex* index of refraction includes effects of currents $\Rightarrow \vec{K} = 0$
- requirements at interface between media 1 and 2

$$
\begin{aligned}
\left(\vec{D}_2 - \vec{D}_1\right) \cdot \vec{n} &= 0 \\
\left(\vec{B}_2 - \vec{B}_1\right) \cdot \vec{n} &= 0 \\
\left(\vec{E}_2 - \vec{E}_1\right) \times \vec{n} &= 0 \\
\left(\vec{H}_2 - \vec{H}_1\right) \times \vec{n} &= 0
\end{aligned}
$$

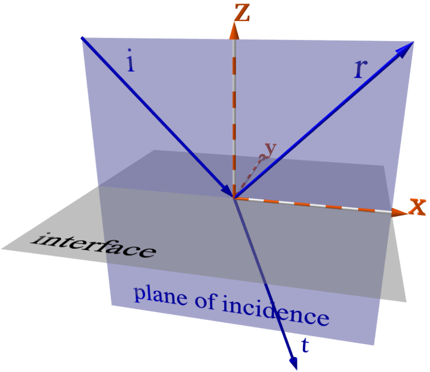
- normal components of $\vec{D}$ and $\vec{B}$ are continuous across interface
- tangential components of $\vec{E}$ and $\vec{H}$ are continuous across interface

Plane of Incidence

- plane wave onto interface
- incident (^{i}), reflected (^{r}), and transmitted (^{t}) waves

$$\vec{E}^{i,r,t} = \vec{E}_0^{i,r,t} e^{i\left(\vec{k}^{i,r,t}\cdot\vec{x}-\omega t\right)}$$
$$\vec{H}^{i,r,t} = \frac{c}{\mu\omega}\vec{k}^{i,r,t} \times \vec{E}^{i,r,t}$$

- interface normal $\vec{n} \parallel z$-axis



- spatial, temporal behavior at interface the same for all 3 waves

$$(\vec{k}^i \cdot \vec{x})_{z=0} = (\vec{k}^r \cdot \vec{x})_{z=0} = (\vec{k}^t \cdot \vec{x})_{z=0}$$

- valid for all $\vec{x}$ in interface $\Rightarrow$ all 3 wave vectors in one plane, *plane of incidence*

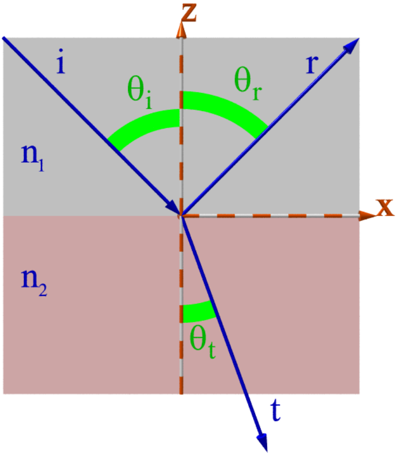
Snell's Law

- spatial, temporal behavior the same for all three waves

$$(\vec{k}^i \cdot \vec{x})_{z=0} = (\vec{k}^r \cdot \vec{x})_{z=0} = (\vec{k}^t \cdot \vec{x})_{z=0}$$

- $\left|\vec{k}\right| = \frac{\omega}{c}\tilde{n}$
- ω, c the same for all 3 waves
- *Snell's law*

$$\tilde{n}_1 \sin\theta_i = \tilde{n}_1 \sin\theta_r = \tilde{n}_2 \sin\theta_t$$



Monochromatic Wave at Interface

- $$\vec{H}_0^{i,r,t} = \frac{c}{\omega\mu}\vec{k}^{i,r,t} \times \vec{E}_0^{i,r,t}, \quad \vec{B}_0^{i,r,t} = \frac{c}{\omega}\vec{k}^{i,r,t} \times \vec{E}_0^{i,r,t}$$
- boundary conditions for monochromatic plane wave:

$$\left(\tilde{n}_1^2 \vec{E}_0^i + \tilde{n}_1^2 \vec{E}_0^r - \tilde{n}_2^2 \vec{E}_0^t\right) \cdot \vec{n} = 0$$

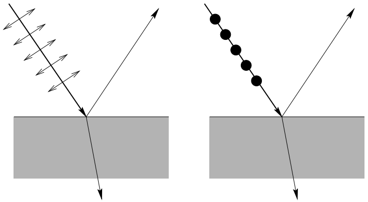
$$\left(\vec{k}^i \times \vec{E}_0^i + \vec{k}^r \times \vec{E}_0^r - \vec{k}^t \times \vec{E}_0^t\right) \cdot \vec{n} = 0$$

$$\left(\vec{E}_0^i + \vec{E}_0^r - \vec{E}_0^t\right) \times \vec{n} = 0$$

$$\left(\frac{1}{\mu_1}\vec{k}^i \times \vec{E}_0^i + \frac{1}{\mu_1}\vec{k}^r \times \vec{E}_0^r - \frac{1}{\mu_2}\vec{k}^t \times \vec{E}_0^t\right) \times \vec{n} = 0$$

- 4 equations are not independent
- only need to consider last two equations (tangential components of $\vec{E}_0$ and $\vec{H}_0$ are continuous)

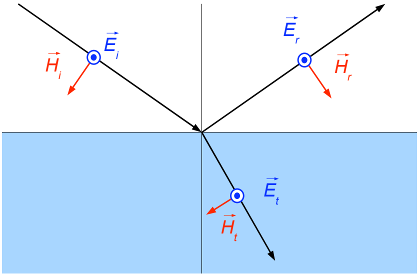
Two Special Cases



1. electric field **p**arallel to plane of incidence $\Rightarrow$ magnetic field is transverse to plane of incidence (TM)
2. electric field particular (German: **s**enkrecht) or transverse to plane of incidence (TE)

- general solution as (coherent) superposition of two cases
- choose direction of magnetic field vector such that Poynting vector parallel, same direction as corresponding wave vector

Electric Field Perpendicular to Plane of Incidence

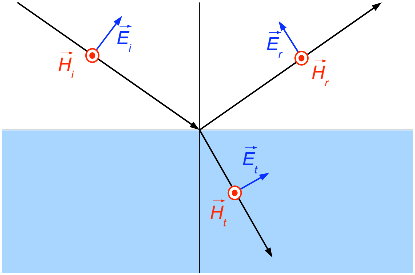


- $\theta_r = \theta_i$
- ratios of reflected and transmitted to incident wave amplitudes

$$r_s = \frac{E_0^r}{E_0^i} = \frac{\tilde{n}_1 \cos\theta_i - \frac{\mu_1}{\mu_2}\tilde{n}_2 \cos\theta_t}{\tilde{n}_1 \cos\theta_i + \frac{\mu_1}{\mu_2}\tilde{n}_2 \cos\theta_t}$$

$$t_s = \frac{E_0^t}{E_0^i} = \frac{2\tilde{n}_1 \cos\theta_i}{\tilde{n}_1 \cos\theta_i + \frac{\mu_1}{\mu_2}\tilde{n}_2 \cos\theta_t}$$

Electric Field in Plane of Incidence



- ratios of reflected and transmitted to incident wave amplitudes

$$r_p = \frac{E_0^r}{E_0^i} = \frac{\tilde{n}_2 \cos\theta_i \frac{\mu_1}{\mu_2} - \tilde{n}_1 \cos\theta_t}{\tilde{n}_2 \cos\theta_i \frac{\mu_1}{\mu_2} + \tilde{n}_1 \cos\theta_t}$$

$$t_p = \frac{E_0^t}{E_0^i} = \frac{2\tilde{n}_1 \cos\theta_i}{\tilde{n}_2 \cos\theta_i \frac{\mu_1}{\mu_2} + \tilde{n}_1 \cos\theta_t}$$

Summary of Fresnel Equations

- eliminate θ_t using Snell's law $\tilde{n}_2 \cos\theta_t = \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}$
- for most materials $\mu_1/\mu_2 \approx 1$
- electric field amplitude transmission $t_{s,p}$, reflection $r_{s,p}$

$$
\begin{aligned}
t_s &= \frac{2\tilde{n}_1 \cos\theta_i}{\tilde{n}_1 \cos\theta_i + \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}} \\
t_p &= \frac{2\tilde{n}_1 \tilde{n}_2 \cos\theta_i}{\tilde{n}_2^2 \cos\theta_i + \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}} \\
r_s &= \frac{\tilde{n}_1 \cos\theta_i - \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}}{\tilde{n}_1 \cos\theta_i + \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}} \\
r_p &= \frac{\tilde{n}_2^2 \cos\theta_i - \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}}{\tilde{n}_2^2 \cos\theta_i + \tilde{n}_1 \sqrt{\tilde{n}_2^2 - \tilde{n}_1^2 \sin^2\theta_i}}
\end{aligned}
$$

Consequences of Fresnel Equations

- complex index of refraction $\Rightarrow t_s, t_p, r_s, r_p$ (generally) complex
- real indices $\Rightarrow$ argument of square root can still be negative $\Rightarrow$ complex t_s, t_p, r_s, r_p
- real indices, arguments of square roots positive (e.g. dielectric without total internal reflection)
    - therefore $t_{s,p} \geq 0$, real $\Rightarrow$ incident and transmitted waves will have same phase
    - therefore $r_{s,p}$ real, but become negative when $n_2 > n_1 \Rightarrow$ negative ratios indicate phase change by 180° on reflection by medium with larger index of refraction

Other Form of Fresnel Equations

- using trigonometric identities

$$
\begin{aligned}
t_s &= \frac{2\sin\theta_t\cos\theta_i}{\sin(\theta_i+\theta_t)} \\
t_p &= \frac{2\sin\theta_t\cos\theta_i}{\sin(\theta_i+\theta_t)\cos(\theta_i-\theta_t)} \\
r_s &= -\frac{\sin(\theta_i-\theta_t)}{\sin(\theta_i+\theta_t)} \\
r_p &= \frac{\tan(\theta_i-\theta_t)}{\tan(\theta_i+\theta_t)}
\end{aligned}
$$

- refractive indices "hidden" in angle of transmitted wave, θ_t
- can always rework Fresnel equations such that only ratio of refractive indices appears
- $\Rightarrow$ Fresnel equations do not depend on absolute values of indices
- can arbitrarily set index of air to 1; then only use indices of media measured relative to air

Relative Amplitudes for Arbitrary Polarization

- electric field vector of incident wave $\vec{E}_0^i$, length E_0^i, at angle α to plane of incidence
- decompose into 2 components: parallel and perpendicular to interface

$$E_{0,p}^i = E_0^i \cos\alpha\,, \quad E_{0,s}^i = E_0^i \sin\alpha$$

- use Fresnel equations to obtain corresponding (complex) amplitudes of reflected and transmitted waves

$$E_{0,p}^{r,t} = (r_p, t_p)\, E_0^i \cos\alpha\,, \quad E_{0,s}^{r,t} = (r_s, t_s)\, E_0^i \sin\alpha$$

Reflectivity

- Fresnel equations apply to electric field amplitude
- need to determine equations for intensity of waves
- time-averaged Poynting vector $\left\langle \vec{S} \right\rangle = \frac{c}{8\pi} \frac{|\tilde{n}|}{\mu} |E_0|^2 \frac{\vec{k}}{|\vec{k}|}$
- absolute value of complex index of refraction enters
- energy along wave vector and not along interface normal
- each wave propagates in different direction $\Rightarrow$ consider energy of each wave passing through unit surface area on interface
- does not matter for reflected wave $\Rightarrow$ ratio of reflected and incident intensities is independent of these two effects
- relative intensity of reflected wave (*reflectivity*)

$$R = \frac{\left|E_0^r\right|^2}{\left|E_0^i\right|^2}$$

Transmissivity

- transmitted intensity: multiplying amplitude squared ratios with
  - ratios of indices of refraction
  - projected area on interface
- relative intensity of transmitted wave (*transmissivity*)

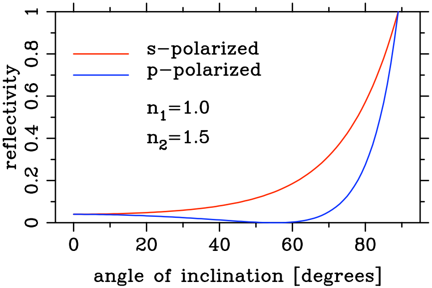
$$T = \frac{|\tilde{n}_2| \cos\theta_t \left|E_0^t\right|^2}{|\tilde{n}_1| \cos\theta_i \left|E_0^i\right|^2}$$

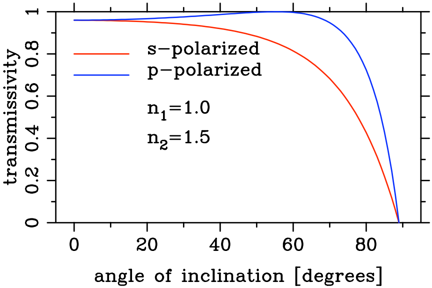
- arbitrarily polarized light with $\vec{E}_0^i$ at angle α to plane of incidence

$$\begin{aligned} R &= |r_p|^2 \cos^2\alpha + |r_s|^2 \sin^2\alpha \\ T &= \frac{|\tilde{n}_2| \cos\theta_t}{|\tilde{n}_1| \cos\theta_i} \left(|t_p|^2 \cos^2\alpha + |t_s|^2 \sin^2\alpha \right) \end{aligned}$$

- $R + T = 1$ for dielectrics, not for conducting, absorbing materials

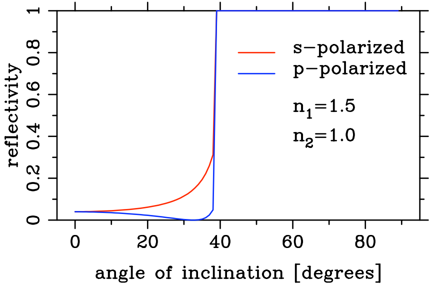
Brewster Angle

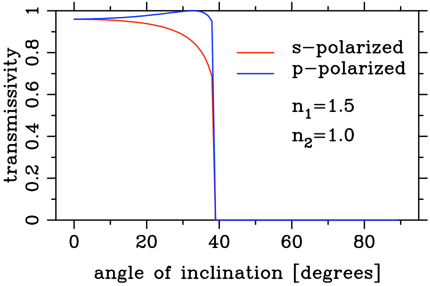




- $r_p = \frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)} = 0$ when $\theta_i + \theta_t = \frac{\pi}{2}$
- corresponds to *Brewster angle* of incidence of $\tan\theta_B = \frac{n_2}{n_1}$
- occurs when reflected wave is perpendicular to transmitted wave
- reflected light is completely s-polarized
- transmitted light is moderately polarized

Total Internal Reflection (TIR)





- Snell's law: $\sin\theta_t = \frac{n_1}{n_2}\sin\theta_i$
- wave from high-index medium into lower index medium (e.g. glass to air): $n_1/n_2 > 1$
- right-hand side > 1 for $\sin\theta_i > \frac{n_2}{n_1}$
- all light is reflected in high-index medium $\Rightarrow$ *total internal reflection*
- transmitted wave has complex phase angle $\Rightarrow$ damped wave along interface

Phase Change on Total Internal Reflection (TIR)

- TIR induces phase change that depends on polarization
- complex ratios: $r_{s,p} = |r_{s,p}|e^{i\delta_{s,p}}$
- phase change $\delta = \delta_s - \delta_p$

$$\tan\frac{\delta}{2} = \frac{\cos\theta_i\sqrt{\sin^2\theta_i - \left(\frac{n_2}{n_1}\right)^2}}{\sin^2\theta_i}$$

- relation valid between critical angle and grazing incidence
- for critical angle and grazing incidence, phase difference is zero